

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
17 January 2002 (17.01.2002)

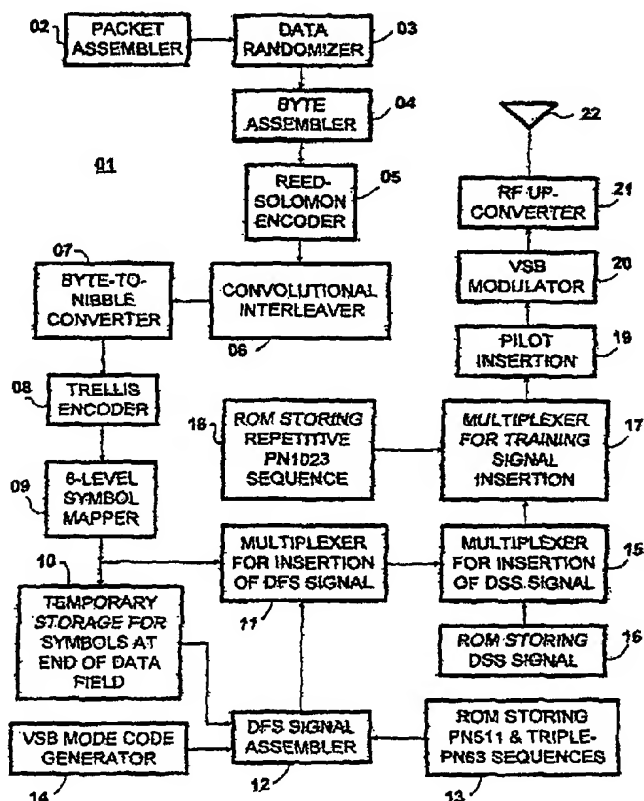
PCT

(10) International Publication Number
WO 02/05555 A1

- (51) International Patent Classification⁷: **H04N 7/015**
- (21) International Application Number: **PCT/KR01/01190**
- (22) International Filing Date: **11 July 2001 (11.07.2001)**
- (25) Filing Language: **English**
- (26) Publication Language: **English**
- (30) Priority Data:
60/217,495 11 July 2000 (11.07.2000) US
60/241,158 18 October 2000 (18.10.2000) US
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- (81) Designated States (national): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, TZ, UA, UG, US, UZ, VN, YU, ZA, ZW.

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(54) Title: REPETITIVE-PN1023-SEQUENCE ECHO-CANCELLATION REFERENCE SIGNAL FOR SINGLE-CARRIER DIGITAL TELEVISION BROADCAST SYSTEMS



(57) Abstract: DTV signals transmitted over the air with a symbol rate of around 10.76 million samples per second include echo-cancellation reference (ECR) signals each of which includes or essentially consists of a repetitive-PN1023 sequence with baud-rate symbols, which repetitive-PN1023 sequence incorporates a number of consecutive data-segment synchronization signals. Receivers for these DTV signals respond to these ECR signals to generate initial weighting coefficients for adaptive filters used for channel equalization and echo suppression. The initial weighting coefficients are calculated from a cepstrum extracted from the repetitive-PN1023 sequence ECR signal by DFT methods or with a PN1023 auto-correlation match filter.



(84) Designated States (regional): ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).

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Published:

— *with international search report*

**REPETITIVE-PN1023-SEQUENCE ECHO-CANCELLATION REFERENCE
SIGNAL FOR SINGLE-CARRIER DIGITAL TELEVISION BROADCAST
SYSTEMS**

5 Technical Field

 The invention relates to digital television (DTV) signals for over-the-air broadcasting, transmitters for such broadcast DTV signals, and receivers for such broadcast DTV signals, which broadcast DTV signals include novel echo-cancellation reference (ECR) signal components for initializing the parameters of
10 adaptive filters used in the DTV receivers for channel-equalization and echo-cancellation.

Background Art

 The Advanced Television Systems Committee (ATSC) published a Digital
15 Television Standard in 1995 as Document A/53, hereinafter referred to simply as "A/53" for sake of brevity. Annex D of A/53 titled "RF/Transmission Systems Characteristics" is particularly incorporated by reference into this specification. Annex D specifies that the data frame shall be composed of two data fields, each data field composed of 313 data segments, and each data segment composed of
20 832 symbols. Annex D specifies that each data segment shall begin with a 4-symbol data-segment-synchronization (DSS) sequence. Annex D specifies that the initial data segment of each data field shall contain a data-field-synchronization (DFS) signal following the 4-symbol DSS sequence therein. The fifth through 515th symbols in each A/53 DFS signal are a specified PN511
25 sequence — that is, a pseudo-random noise sequence composed of 511 symbols capable of being rendered as +5 or -5 values. The 516th through 704th symbols in each A/53 DFS signal are a triple-PN63 sequence composed of a total of 189 symbols capable of being rendered as +5 or -5 values. The middle PN63 sequence is inverted in polarity every other data field. The 705th through
30 728th symbols in each A/53 DFS signal contain a VSB mode code specifying the

nature of the vestigial-sideband (VSB) signal being transmitted. The remaining 104 symbols in the each A/53 DFS signal are reserved, with the last twelve of these symbols being a precode signal that repeats the last twelve symbols of the data in the last data segment of the previous data field. A/53 specifies such
5 precode signal to implement trellis coding and decoding procedures being able to resume in the second data segment of each field proceeding from where those procedures left off processing the data in the preceding data field.

The broadcast TV signal to which the receiver synchronizes its operations is called the principal signal, and the principal signal is usually the direct signal
10 received over the shortest transmission path. Thus, the multipath signals received over other paths are usually delayed with respect to the principal signal and appear as lagging ghost signals. It is possible however, that the direct or shortest path signal is not the signal to which the receiver synchronizes. When the receiver synchronizes its operations to a (longer path) signal that is delayed
15 respective to the direct signal, there will be a leading multipath signal caused by the direct signal, or there will a plurality of leading multipath signals caused by the direct signal and other reflected signals of lesser delay than the reflected signal to which the receiver synchronizes. In the analog TV art multipath signals are referred to as "ghosts", but in the DTV art multipath signals are customarily
20 referred to as "echoes". The multipath signals that lead the principal signal are referred to as "pre-echoes", and the multipath signals that lag the principal signal are referred to as "post-echoes". The echoes vary in number, amplitude and delay time from location to location and from channel to channel at a given location. Post-echoes with significant energy have been reported as being
25 delayed from the reference signal by as many as sixty microseconds. Pre-echoes with significant energy have been reported leading the reference signal by as many as thirty microseconds. This 90-microsecond or so possible range of echoes of is appreciably more extensive than was generally supposed before spring 2000.

30 The transmission of the digital television (DTV) signal to the receiver is considered to be through a transmission channel that has the characteristics of a

sampld-data time-domain filter that provides weighted summation of variously delayed responses to the transmitted signal. In the DTV signal receiver the received signal is passed through equalization and echo-cancellation filtering that compensates at least partially for the time-domain filtering effects that originate in the transmission channel. This equalization and echo-cancellation filtering is customarily sampled-data filtering performed in the digital domain. Time-domain filtering effects differ for the channels through which broadcast digital television signals are received from various transmitters. Furthermore, time-domain filtering effects change over time for the broadcast digital television signals received from each particular transmitter. Changes referred to as "dynamic multipath" are introduced while receiving from a single transmitter when the lengths of reflective transmission paths change, owing to the reflections being from moving objects. Accordingly, adaptive filtering procedures are required for adjusting the weighting coefficients of the sampled-data filtering that provides echo-cancellation and equalization.

Determination of the weighting coefficients of the sampled-data filtering that provides equalization and echo-cancellation is customarily attempted using a method of one of two general types. A method of the first general type relies on analysis of the effects of multipath just on an ECR signal or echo-cancellation reference (ECR) signal included in the transmitted signal specifically to facilitate such analysis. A method of the second general type relies on analysis of the effects of multipath on all portions of the transmitted signal. While the PN511 and triple-PN63 sequences in the initial data segments of the data fields in the ATSC standard DTV signal were originally proposed for use as ECR signals, the VSB receiver performance in actual field environments has demonstrated that these sequences are inadequate ECR signals, considered separately or in combination. So, most DTV manufacturers have used decision-feedback methods that rely on analysis of the effects of multipath on all portions of the transmitted signal for adapting the weighting coefficients of the sampled-data filtering. Decision-feedback methods that utilize least-mean-squares (LMS) method or block LMS method can be implemented in an integrated circuit of

reasonable size. These decision-feedback methods provide for tracking dynamic multipath conditions reasonably well after the equalization and echo-cancellation filtering has initially been converged to substantially optimal response, providing that the sampling rate through the filtering is appreciably higher than symbol rate, and providing that the rate of change of the dynamic multipath does not exceed the slewing rate of the decision-feedback loop.

However, these decision-feedback methods tend to be unacceptably slow in converging the equalization and echo-cancellation filtering to nearly optimal response when initially receiving a DTV signal that has bad multipath distortion. Bad multipath distortion conditions include cases where echoes of substantial energy lead or lag the principal received signal by more than ten or twenty microseconds, cases where there is an ensemble of many echoes with differing timings relative to the principal received signal, cases where multipath distortion changes rapidly, and cases where it is difficult to distinguish principal received signal from echo(es) because of similarity in energy level.

Worse yet, convergence is too slow when tracking of dynamic multipath conditions must be regained after the slewing rate of the decision-feedback loop has not been fast enough to keep up with rapid change in the multipath conditions. Data-dependent equalization and echo-cancellation methods that provide faster convergence than LMS or block-LMS decision-feedback methods are known, but there is difficulty in implementing them in an integrated circuit of reasonable size.

Accordingly, it is desirable to modify the A/53 DTV signal to introduce periodically an ECR signal that will "instantly" converge the equalization and echo-cancellation filtering to substantially optimal response. It would be desirable to have an ECR signal that does not interfere with the operation of DTV signal receivers already in the field. However, because of the de-interleaving of VSB-8 signals in the DTV receiver, this is probably an impossible condition to satisfy, at least completely.

U. S. patent application No. 09/776,019 filed by A. L. R. Limberg on January 18, 2001 and titled "GHOST CANCELLATION REFERENCE SIGNALS FOR BROADCAST DIGITAL TELEVISION SIGNAL RECEIVERS AND RECEIVERS FOR UTILIZING THEM" describes each data field being extended
5 a prescribed number of data segments to permit the inclusion of ECR signals composed of repetitive-PN511 sequences with baud-rate symbols. Application No. 09/776,019 also specified that the precode signal repeat the last twelve symbols of the 313th data segment, just as in the standard VSB-8 DTV signal. Extension of the data field to include more than 313 data segments minimizes
10 the modifications of the convolutional interleaver in the DTV transmitter and of the corresponding de-interleaver in the DTV receiver that would have to be made in newly designed DTV receivers. However, the extended data fields will interfere with the operation of some receivers already in the field.

Application No. 09/776,019 pointed out that ECR signal should have
15 sufficient energy that match filtering using auto-correlation procedures can distinguish the longest delayed echoes of the ECR signal from interference caused by other signals and by noise. Accordingly, ECR signals with substantial energy and well-defined auto-correlation responses are a desideratum. The triple PN63 sequence in the initial data segment of each data field of an A/53
20 broadcast DTV signal has a well-defined auto-correlation response, but has insufficient energy for detecting longer-delayed post-echoes with smaller amplitudes. The PN511 sequence in the initial data segment of each data field of an A/53 broadcast DTV signal has substantial energy and a well-defined auto-correlation response. However, no component sequence of the data field
25 synchronizing (DFS) signal or combination of its component sequences has proven in practice to be very satisfactory as an ECR signal.

One reason is that no portion of the DFS signal is preceded by an information-free interval of sufficient duration that post-echoes of previous data and data segment synchronizing sequences exhibit insignificant spectral energy
30 during the duration of that portion of the DFS signal to be used as ECR signal. Also, the A/53 DTV signals do not provide for the generation of an information-

free interval of such duration before the ECR signal by combining information sent at different times, a technique used in de-ghosting NTSC analog television signals. A 60-microsecond-long information-free interval extending over 646 symbol epochs should precede the ECR signal if it is not to be overlapped by the

5 post-echoes of previous signals, which post-echoes can have significant energy if delayed no more than sixty microseconds or so. The post-echoes of previous signals should be kept from contributing significantly to digitized Johnson noise, in order to preserve the sensitivity of echo detection. Similarly, no portion of the DFS signal is succeeded by an information-free interval of sufficient duration that

10 pre-echoes of subsequent data and data segment synchronizing sequences exhibit insignificant spectral energy during the duration of that portion of the DFS signal to be used as ECR signal. A 30-microsecond-long information-free interval extending over 323 symbol epochs should succeed the ECR signal if it is not to be overlapped by the pre-echoes of previous signals, which pre-echoes

15 can have significant energy if advanced no more than thirty microseconds or so. These information-free intervals preferably should be of even longer durations if auto-correlation filtering employing linear convolution is to be used for echo detection.

Another reason the PN511 sequence in the initial data segment of each

20 data field of an ATSC broadcast DTV signal is not particularly satisfactory as an ECR signal is that the PN511 sequence is not repetitive. Therefore, the auto-correlation properties of the PN511 sequence are compromised. The reader is referred to U. S. patent No. 5,065,242 titled "DEGHOSTING APPARATUS USING PSEUDORANDOM SEQUENCES" issued 23 August 1994 to Charles

25 Dietrich and Arthur Greenberg. This patent, incorporated herein by reference, points out that the auto-correlation function of a maximal-length pseudorandom noise (PN) sequence has a cyclic nature. The patent describes repetitive PN sequences being inserted as ECR signal into a prescribed scan line interval of each of the vertical blanking intervals of NTSC analog television signals. U. S.

30 patent No. 5,065,242 describes the transmission/reception channel

characterization being performed using fast Fourier transform (FFT) or discrete Fourier transform (DFT) methods.

5 The 90-microsecond or so possible range of echoes that is now known to exist in actual practice is appreciably more extensive than A. L. R. Limberg presumed when on 19 January 2000 he filed provisional U. S. patent application serial No. 60/178,081, the priority document for U. S. patent application No. 09/776,019. Limberg presumed an echo range of only 45 microseconds or so, and the ECR signals specifically described relied on repetitive PN511 sequences with baud-rate symbols rendered as +5 or -5 values. Limberg described the
10 repetitive PN511 sequences being chosen such that they incorporated the +5, -5, -5, +5 symbol sequences at 832-symbol-epoch intervals, which sequences are used as data segment synchronizing (DSS) signals in DTV transmissions made in accordance with A/53. Baud-rate repetitive PN511 sequences are capable of unambiguous detection of echoes over a range of less than 47.5 microseconds.

15 In spring 2000, when it was reported to the ATSC Task Force on RF System Performance that the range of echoes with significant energy apt to be encountered in the field could be 90 microseconds or so wide, A. L. R. Limberg realized that unambiguous detection of echoes over so wide a range would be facilitated by ECR signals that employed baud-rate repetitive PN1023 sequences.
20 The question was whether repetitive PN1023 sequences existed that incorporated the +5, -5, -5, +5 DSS sequences at four consecutive 832-symbol-epoch intervals. While he doubted that such repetitive PN1023 sequence existed, A. L. R. Limberg asked this question of the ATSC Task Force on RF System Performance using e-mail, indicating he did not have the software for calculating
25 all PN1023 sequences, replicating them and sifting the results.

Surprisingly, D. J. McDonald replied via e-mail later the same day that certain repetitive PN1023 sequences did indeed meet this criterion and that a number of others incorporated the +5, -5, -5, +5 DSS sequences at a lesser number of consecutive 832-symbol-epoch intervals. D. J. McDonald found
30 sequences of the type desired by writing a program for sifting through an already

existent file found on-line. More DSS sequences have to be subsumed by a repetitive-PN sequence as n increases beyond 8 or so, but this problem is not as difficult as it first appears. As the (P^n-1) length of a pseudo-random noise (PN) sequence increases with increase in the number n , the number of sequences
5 increases more than linearly.

Further aspects of the invention concerned exactly how to incorporate the 3096-symbol-epoch triple-PN1023 sequence into the ATSC standard broadcast signal inasmuch as more than three data segments would be required to contain the entire 3096 symbol sequence. C. B. Patel suggested that the DFS signal be
10 modified, eliminating the PN511 sequence and the initial PN63 sequence to leave room for the tail of a 3096-symbol-epoch triple-PN1023 sequence beginning the third from final data segment of the previous data field. A. L. R. Limberg suggested that the DFS signal be modified, eliminating the PN511 sequence but retaining the initial PN63 sequence, and that the triple-PN1023
15 sequence be truncated to 3011 symbol epochs. This would still permit linear convolution of a PN1023 auto-correlation filter with the received repetitive-PN1023 sequence to detect without ambiguity echoes extending over a 90-microsecond range.

A. L. R. Limberg and C. B. Patel wanted to truncate the repetitive-PN1023
20 sequence even further to 2500 symbol epochs, so it could be fitted into three consecutive data segments. This would facilitate leaving the DFS signal in the ATSC standard intact, but would reduce to less than the desired 90 microseconds the range of echoes that could be detected without ambiguity by simply passing the received repetitive PN1023 sequence through a PN1023
25 auto-correlation filter in a simple linear convolution procedure. D. J. McDonald pointed out that the cyclic nature of the repetitive PN1023 sequence meant that all the echo information required for DFT procedures for characterizing the channel reposed in a interior cycle of the PN1023 sequence overlapped only by echoes of itself and flanking PN1023 signal. This permits DFT procedures to
30 detect echoes without ambiguity over an echo range approaching 95 microseconds width, so long as there are at least two cycles of PN1023

sequence in the ECR signal. The interior cycle of the PN1023 sequence can be looped back on itself to extend the sequence in length for calculation purposes.

When A. L. R. Limberg relayed this observation to C. B. Patel, Dr. Patel discerned that looping an interior cycle of the PN1023 sequence back on itself permitted circular convolution with the kernel of a PN1023 auto-correlation filter, for detecting echoes without ambiguity over an echo range approaching 95 microseconds width, so long as there are at least two cycles of PN1023 sequence in the ECR signal.

10 Disclosure of the Invention

Aspects of the invention concern incorporating echo-cancellation reference (ECR) signals into a DTV signal with a symbol rate of around 10.76 million samples per second, wherein each of the ECR signals includes or essentially consists of a repetitive-PN1023 sequence with baud-rate symbols rendered as +5 or -5 values, which repetitive-PN1023 sequence incorporates a number of consecutive data-segment-synchronization signals. Other aspects of the invention concern transmitters and receivers for such signals.

Brief Description of the Drawings

20 FIGURES 1A and 1B together are a listing, row by row, left to right, of the symbols in a repetitive-PN1023 sequence that is used in generating broadcast digital television signals transmitted in accordance with an aspect of the invention.

FIGURE 2 is a diagram of an ATSC digital television signal data frame modified in accordance with an aspect of the invention to include three extra data segments at the end of each of its two data fields, which extra segments contain a repetitive-PN1023-sequence training signal for the adaptive filtering that provides channel-equalization and echo-cancellation.

FIGURES 3A, 3B, 3C, 3D, 3E, 3F, 3G, 3H, 3I, 3J, 3K and 3L are timing diagrams that depict the symbol content of respective data segments in

broadcast digital television signals transmitted in accordance with an aspect of the invention.

FIGURE 4 is a block schematic diagram of a transmitter for transmitting broadcast digital television signals in accordance with an aspect of the invention.

5 FIGURE 5 is a schematic diagram of a portion of a receiver for broadcast digital television signals, which receiver portion includes an adaptive filter for providing channel-equalization and echo-suppression at baseband, and which receiver portion in accordance with a further aspect of the invention includes apparatus utilizing the signal of FIGURES 3A, 3B, 3C, 3D, 3E, 3F, 3G, 3H, 3I, 3J,
10 3K and 3L in DFT computations used in calculating weighting coefficients for the adaptive filter.

FIGURE 6 is a schematic diagram of a portion of another receiver for broadcast digital television signals, which receiver portion includes an adaptive filter for providing channel-equalization and echo-suppression at baseband, and
15 which receiver portion in accordance with a further aspect of the invention includes structure capable of utilizing the signal of FIGURES 3A, 3B, 3C, 3D, 3E, 3F, 3G, 3H, 3I, 3J, 3K and 3L in auto-correlation filtering procedures used in calculating weighting coefficients for the adaptive filter.

20 FIGURE 7 is a schematic diagram of a further portion of a receiver for broadcast digital television signals, as may follow the portion of the receiver shown in either of the FIGURES 5 and 6.

FIGURE 8A is a graph versus time of the cyclically repeating cepstrum of a signal received under multipath reception conditions, as that cepstrum is
25 determined in the receiver portion of FIGURE 5 or in the receiver portion of FIGURE 6.

FIGURES 8B, 8C and 8D are each a graph plotted against the same time scale as FIGURE 8A showing successive steps in unwrapping the cyclically repeating cepstrum of FIGURE 8A to develop an extended cepstrum.

FIGURE 9 is a block schematic diagram of apparatus that can be used in accordance with an aspect of the invention for further analyzing the cepstrum of the received DTV signal.

FIGURES 10A, 10B and 10C are graphs, versus the same time abscissa, of time-domain responses at points in circuitry in the FIGURE 9 apparatus used for further analyzing the pre-echo portion of the cepstrum.

FIGURES 10D, 10E and 10F are graphs, versus the same time abscissa, of time-domain responses at points in additional circuitry in the FIGURE 9 apparatus used for further analyzing the post-echo portion of the cepstrum.

FIGURE 11 is a diagram of an ATSC digital television signal data frame modified in accordance with an aspect of the invention to include 315 data segments in each of its two data fields, to omit the A/53 data field synchronization signal in the first data segment of each data field, and to include in each data field a training signal for the adaptive filtering that provides channel-equalization and echo-cancellation, which training signal is a repetitive-PN1023 sequence also employed as a data field synchronization signal.

FIGURES 12A, 12B, 12C, 12D, 12E, 12F, 12G, 12H, 12I and 12J are timing diagrams that depict the symbol content of respective data segments in broadcast digital television signals of the type shown in FIGURE 11.

Best mode for carrying out the Invention

FIGURES 1A and 1B together provide a listing, row by row, left to right, of the consecutive symbols in a 2507-symbol repetitive-PN1023 sequence that can be used in implementing the invention in various of its aspects. The ONES in the 2507-symbol repetitive-PN1023 sequence correspond to +5 carrier modulation

values in the digital television signal, and the ZEROs in the 2507-symbol repetitive-PN1023 sequence correspond to -5 carrier modulation values. The repetitive-PN1023 sequence is used for modulating the vestigial-sideband carrier during the 314th, 315th and 316th data segments that conclude each data field and during the first eleven symbols in the initial data segment of the next data field. The repetitive-PN1023 sequence begins with a 1001 sequence that modulates the vestigial-sideband carrier as a data segment synchronizing (DSS) signal and has other such sequences 832, 1664 and 2496 symbol epochs later. Except for these DSS signals, modulation of the vestigial-sideband carrier in accordance with the repetitive-PN1023 sequence does not otherwise contain +5, -5, -5, +5 sequence at similar positioning in 832-symbol data segments. If the order of the symbols in the FIGURE 1 repetitive-PN1023 sequence is reversed, these favorable properties still obtain. There are more than these two PN1023 sequences with the described desirable properties, J. D. McDonald having found two families of them. The particular repetitive-PN1023 sequence shown in FIGURES 1A and 1B is preferred since it overlaps the PN511 sequence in the initial data segment by seven symbol epochs, the longest overlap of any known repetitive-PN1023 sequence.

FIGURE 2 is a diagram of an ATSC digital television signal data frame modified to include three extra data segments at the end of each of its two data fields. The initial data segment in each data field is the same as specified by A/53, the final twelve symbols from the 313th data segment of each data field being used to form the precode concluding the first data segment of the next data field. Repetitive-PN1023 sequence training signal for equalization and echo-cancellation filtering is included in the three additional data segments in each data field and in several embodiments of the invention a portion of the first data segment of the next data field. In the embodiment of the invention described above the repetitive-PN1023 sequence overlaps the PN511 sequence in the initial data segment by seven symbol epochs. In other embodiments of the invention the conclusion of the training signal replaces one or more of the

pseudo-random-noise (PN) sequences in the first data segment of each data field.

At the DTV transmitter the operations of the interleaver and trellis coder are suspended during the transmission of the 314th, 315th and 316th data segments added to each data field, as well as during the initial data segment of each data field. At these times the operations of the trellis decoder and of the de-interleaver in a DTV receiver especially designed for receiving the FIGURE 2 broadcast digital television signal are also suspended. A DTV receiver designed to receive DTV signals broadcast in accordance with the 1995 ATSC Standard is unlikely to be designed such that the operations of the trellis decoder and of the de-interleaver are suspended during the 314th, 315th and 316th data segments added to each data field. If the operations of the trellis decoder and of the de-interleaver are not so suspended, the de-interleaved data will contain errors that cannot be corrected by the Reed-Solomon error-correction circuitry following the de-interleaver.

FIGURES 3A, 3B, 3C and 3D depict the symbol content of the 313th, 314th, 315th and 316th data segments of the even data field of a previous data frame in a FIGURE 2 DTV signal broadcast in accordance with the invention. FIGURES 3E and 3F graph the symbol content of the initial and second data segments of the succeeding odd data field in the current data frame. FIGURES 3G, 3H, 3I and 3J depict the symbol content of the 313th, 314th, 315th and 316th data segments of that succeeding odd data field. FIGURES 3K and 3L graph the symbol content of the initial and second data segments data segment of the even data field of the next data frame.

The second through 313th data segments of the data fields can be the same as those specified in A/53. The third through 312th data segments of the odd field of the current frame, which would occur in the time interval between the conclusion of the second data segment shown in FIGURE 3F and the beginning of the 313th data segment shown in FIGURE 3G are omitted from the drawing for reasons of economy of drawing.

The 314th, 315th and 316th data segments concluding each data field contain the first 2496 symbols of the repetitive-PN1023-sequence ECR signal, which continues into the initial data segments of the succeeding data fields. FIGURES 3B, 3C and 3D show the first 2496 symbols of the repetitive-PN1023-sequence ECR signal inserted into the 314th, 315th and 316th data segments of the even data field of the data frame previous to the current data frame depicted in FIGURES 3E, 3F, 3G, 3H, 3I, and 3J. FIGURES 3H, 3I and 3J show the first 2496 symbols of the repetitive-PN1023-sequence ECR signal inserted into the 314th, 315th and 316th data segments of the odd data field of the current data frame. The data segment synchronizing (DSS) signals of the 314th, 315th and 316th data segments of each data field are incorporated within the repetitive-PN1023-sequence ECR signal transmitted during those data segments. So is the DSS signal at the beginning of the initial data segment of the succeeding field, and so are the first seven symbols of the PN511 component of that initial data segment, as depicted in FIGURES 3E and 3K.

The repetitive-PN1023 sequence of FIGURES 3B, 3C, 3D and 3E varies between -5 and +5 modulation levels in the 8-VSB signal, as A/53 specifies such modulation levels. The repetitive-PN1023 sequence of FIGURES 3H, 3I, 3J and 3K also varies between -5 and +5 modulation levels. These modulation levels for the repetitive-PN1023 sequences facilitate the 4-symbol DSS sequences being incorporated within these repetitive-PN1023 sequences.

The initial data segment of an odd data field, as shown in FIGURE 3E, and the initial data segment of a succeeding even data field, as shown in FIGURE 3K, each begin with a 4-symbol data segment sync (DSS) sequence followed by the PN511 sequence prescribed by A/53. The conclusion of the repetitive-PN1023 sequence is followed by a 189-symbol triple PN63 sequence, a 24-symbol mode code, and a 104-symbol reserved portion that concludes the data segment. In FIGURE 3K the PN511 sequence is followed by a 189-symbol triple PN63 sequence differing from that in FIGURE 3E in that the middle PN63 sequence in the triple PN63 sequence is opposite in sense of polarity to the other PN63 sequences.

FIGURE 4 shows a digital television transmitter **01** for transmitting broadcast digital television signals in accordance with an aspect of the invention. The transmitter **01** includes a packet assembler **02** of conventional type for assembling packets of MPEG-2 Standard video data, packets of AC-3 Standard audio data, and packets of other data into a data stream. The packet assembler **02** is sometimes called the "transport- stream multiplexer". The packet assembler **02** is connected to supply the data stream it assembles to a data randomizer **03** of the type specified in A/53, Annex D, Section 4.2.2. The data randomizer **03** exclusive-ORs all the incoming data with a $(2^{17}-1)$ -symbol maximal-length PN sequence, which is initialized at the beginning of each data field. The data randomizer **03** is connected for supplying randomized data to a byte assembler **04**. The byte assembler **04** is connected for supplying randomized data in eight-bit bytes to a Reed-Solomon coder **05** of (207, 187) type as specified in A/53, Annex D, Section 4.2.3. The Reed-Solomon coder **05** is connected to a convolutional interleaver **06** for supplying it bytes of randomized data with forward-error-correction codes inserted therein. The convolutional interleaver **06** supplies bytes of interleaved data descriptive of data segments 2 through 313 of each interleaved data field that is to be transmitted.

The convolutional interleaver **06** is connected to supply these bytes of interleaved data to a byte-to-nibble converter **07**, which converts those bytes to a stream of two-bit nibbles. The byte-to-nibble converter **07** is connected to supply this nibble stream to a trellis encoder **08**, which performs 2/3 rate trellis coding of the type prescribed in A/53. The trellis encoder **08** is connected to supply its trellis-coded output signal to an 8-level symbol mapper **09** of the type prescribed in A/53. The last twelve symbols resulting from data segment 313 of the interleaved data field are stored temporarily in temporary storage register **10**, to be used subsequently as precode at the conclusion of the initial data segment of the next data field.

A time-division multiplexer **11** is connected for receiving symbols from the symbol mapper **09**. The time-division multiplexer **11** inserts a data field synchronization (DFS) signal into the trellis-coded signal before data segment 2

of each transmitted data field. The multiplexer **11** is connected for receiving the DFS signal from a DFS signal assembler **12**. The DFS signal assembler **12** assembles the PN511 and triple-PN63 sequences read from a read-only memory **13** at the beginning of the DFS signal, a VSB mode code supplied from a VSB mode code generator **14** or permanently wired, a "reserved" signal if available, and the precode stored in the temporary storage register **10**.

The time-division multiplexer **11** is connected for supplying its output signal to another time-division multiplexer **15**. The time-division multiplexer **15** inserts a data segment synchronization (DSS) signal at the beginning of each data segment of each transmitted data field. As shown in FIGURE 4, the DSS signal can by way of example be supplied to the multiplexer **15** from a read-only memory **16** read from at suitable times.

In FIGURE 4 the time-division multiplexer **15** is connected for supplying its output signal to still another time-division multiplexer **17**. The time-division multiplexer **17** is designed so that its output signal reproduces the time-division multiplexer **15** output signal with the following modification. ECR signal read from a read-only memory **18** is inserted into the multiplexer **17** output signal following data segment 313 of each transmitted data field.

FIGURE 4 shows pilot insertion circuitry **19** connected for receiving the time-division multiplexer **17** output signal. The pilot insertion circuitry **19** adds a direct component to the multiplexer **17** output signal to generate a modulating signal input for a vestigial-sideband modulator **20** that includes a balanced modulator in its construction. The direct component unbalances the balanced modulator, so the VSB modulator **20** output signal includes a pilot carrier at the carrier frequency. Alternatively, the pilot insertion can be done after modulation. In most commercial DTV transmitter designs the VSB modulator **20** output signal is at an intermediate frequency. A radio-frequency up-converter **21** converts this VSB modulator **20** output signal upward in frequency to the allocated radio-frequency transmission channel in the VHF or UHF band and amplifies the power of the radio-frequency signal applied to a transmitting antenna **22**.

The FIGURE 4 arrangement is most simply clocked at baud rate beginning with the byte-to-nibble converter **07** output signal, introducing nulls into appropriate portions of the convolutional interleaver **06** output signal to accommodate insertions by the time-division multiplexers **11**, **15** and **17**. As one skilled in the art of electronic design will readily perceive, time-division-multiplexer circuitry other than that using multiplexers **11**, **15** and **17** connected per FIGURE 4 can be used for generating a modulating signal by inserting a data field synchronization signal into the trellis-coded signal for each transmitted data field, for inserting a data segment synchronization signal into each data segment of each transmitted data field, and for inserting a non-trellis-coded signal descriptive of the repetitive PN1023 sequence into a prescribed portion of each transmitted data field. One can modify the ROM **18** to store the repetitive-PN1023-sequence ECR signal exclusive of the DSS sequences and reverse the order in which the time-division multiplexers **15** and **17** are cascaded, for example. This facilitates addressing the ROMs **13** and **18** from a common address counter. Another design possibility is to insert DSS signals into the output signals of the symbol mapper **08** and DFS signal assembler **12** independently, before the time-division multiplexer **17** inserts the repetitive PN1023 sequence ECR signal read periodically from the ROM **18**.

FIGURE 5 shows a receiver for broadcast DTV signals capable of utilizing repetitive-PN1023-sequence training signals included in those broadcast DTV signals. A source **30** of radio-frequency vestigial-sideband DTV signal, such as a reception antenna, supplies that VSB DTV R-F signal to a DTV receiver front-end **31** comprising tuner and intermediate-frequency (I-F) amplifier stages. The DTV receiver front-end **31** supplies amplified I-F signal to demodulator and analog-to-digital conversion circuitry **32**. The circuitry **32** can take any one of a variety of known forms. Forms of the circuitry **32** in which the amplified I-F signal is digitized by an analog-to-digital converter before demodulation is done in the digital regime are preferred. Alternatively, forms of the circuitry **32** in which demodulation is done in the analog regime with the analog baseband demodulation result subsequently being digitized by an analog-to-digital

converter are used instead. The analog-to-digital conversion is performed at a rate higher than the baud rate, so that the phase modulation of received signal that occurs during dynamic multipath reception can be tracked.

Performing the analog-to-digital conversion at a multiple of baud rate is
5 advantageous, because having an integral number of samples per symbol epoch simplifies the design of digital filters in the receiver. Decimation filtering to baud rate before data slicing is facilitated, for example. Auto-correlation filters for PN sequences can be constructed without need for digital multipliers, by way of further example. Adaptive filtering to perform fractional equalization is facilitated
10 as well.

Demodulator and analog-to-digital conversion circuitry **32** supplies digitized baseband DTV signal. Although FIGURE 5 does not explicitly show it, in line with conventional practice this digitized baseband DTV signal is subjected to band-shaping filtering including Nyquist-slope filtering before its application as
15 input signal to adaptive filtering used for channel-equalization and echo-cancellation, which adaptive filtering can take a variety of known forms. FIGURE 5 shows a representative form of the adaptive filtering, which comprises a first finite-impulse-response (FIR) filter **33** with adjustable weighting coefficients followed in cascade by an infinite-impulse-response (IIR) filter composed of
20 elements **34 - 38**. The response of the first FIR filter **33** is supplied as the IIR filter input signal, which is applied as minuend input signal to a subtractor **34** in the IIR filter. The subtrahend input signal to the subtractor **34** is the response of a second FIR filter **35** with adjustable weighting coefficients. The subtractor **34** supplies its difference output signal as the IIR filter output signal, which is
25 supplied as input signal to the rest **39** of the DTV receiver per conventional practice. Further on in this specification the rest **39** of the DTV receiver is described in detail with reference to FIGURE 7 of the drawing.

The IIR filter output signal is processed for application as input signal to the second FIR filter **35**, completing a degenerative feedback loop through the
30 second FIR filter **35**, the subtractor **34** and intervening elements **36 - 38**. This

feedback loop provides the iterative filtering that gives rise to "infinite" impulse response. Alternatively, "infinite" impulse response could be obtained by directly applying the difference output signal from the subtractor **34** to the second FIR filter **35** as its input signal. However, adjustment of the weighting coefficients of the FIR filters **33** and **35** by data-directed methods is facilitated by replacing the filtered received signal by an estimation of the actually transmitted signal based on the filtered received signal. The output signal of the adaptive filtering for performing equalization and echo-cancellation, which is supplied as difference output signal from the subtractor **34**, is sampled at a rate higher than baud rate, preferably a multiple of baud rate. A decimation filter **36** responds to the difference output signal from the subtractor **34** to supply a quantizer **37** an input signal at baud rate. The quantizer **37** generates, at baud rate, estimates of the symbols actually transmitted. These estimates are applied as input signal to an interpolation filter **38** which resamples them to the same sample rate as the difference output signal from the subtractor **34**. The interpolation filter **38** response is applied to the second FIR filter **35** as its input signal.

A small dedicated computer **40** computes weighting coefficients that are supplied to weighting-coefficient registers for the FIR filters **33** and **35**. (FIGURE 5 does not show these weighting-coefficient registers separately.) Whenever the DTV receiver is powered up after not receiving power for some time, whenever the reception channel is changed, or whenever the error-correction circuitry indicates a current set of weighting coefficients to be seriously in error, a set of weighting coefficients that have been derived from the repetitive-PN1023-sequence training signal are loaded into the computer **40**. This set of weighting coefficients is then supplied to the weighting-coefficient registers for the FIR filters **33** and **35**, as well as providing a basis for the computer **40** further adjusting the weighting coefficients by a data-directed method utilizing a decision-feedback error signal generated by a digital subtractor **41** as its difference output signal. The digital subtractor **41** generates the decision-feedback error signal by comparing the output signal of the adaptive filtering for performing equalization and echo-cancellation with estimates of the actually

transmitted signal as resampled by the interpolation filter **38**. More particularly, the response of the interpolation filter **38** is supplied to the subtractor **41** as its subtrahend input signal, and the difference output signal from the subtractor **34** is delayed by a digital delay line **42** before being applied to the subtractor **41** as its minuend input signal. The delay line **42** delays the subtractor **34** difference output signal sufficiently to compensate for the combined latent delays through the decimation filter **36**, the quantizer **37** and the interpolation filter **38**. The sampling rate of the decision-feedback error signal that the subtractor **41** generates as its difference output signal corresponds with the fractional-symbol tap spacing of the weighting coefficients of the FIR filters **33** and **35**.

Of particular interest to the invention is the way that a set of weighting coefficients is determined from the repetitive-PN1023-sequence training signal depicted in FIGURES 3B, 3C, 3D, 3E, 3H, 3I, 3J and 3K. Demodulator and analog-to-digital conversion circuitry **32** supplies digitized baseband DTV signal to gating circuitry **43**, similar to the digitized baseband DTV signal supplied to the adaptive filtering used for channel-equalization and echo-cancellation. The gating circuitry **43** selects to a computer **44** a 1023-symbol-epoch portion of the digitized baseband DTV signal from the 314th, 315th and 316th data segments of each data field. This 1023-symbol-epoch portion is chosen to occur after the disappearance of the longest-delayed post-echo of the data in the 310th segment, but before the appearance of the earliest pre-echo of the DFS signal in the initial data segment of the succeeding data field. Starting the 1023-symbol-epoch portion in the 312th data segment means that post-echoes of the data in the 310th segment that are delayed less than 78.3 microseconds are all past. Starting the 1023-symbol-epoch portion at the very beginning of the 312th data segment would require that pre-echoes of the DFS signal in the initial data segment of the succeeding data field be advanced a little over 59.5 microseconds in order to overlap such 1023-symbol-epoch portion. Starting the 1023-symbol-epoch portion just after the DSS sequence in the 312th data segment is preferred inasmuch as it facilitates that DSS sequence enabling a counter used for timing

the gating of the selected 1023-symbol-epoch portion to an input storage register in the computer **44**.

The computer **44** is a small computer dedicated for calculating the DFT power spectrum of the portion of the 1023-symbol-epoch portion of digitized baseband DTV signal that the gating circuitry **43** selects to the computer **44**. These power spectrum calculations are performed after resampling the selected signal so the set of samples supplied for DFT calculation contains a number of samples that is an integral power of two. DFT calculation is facilitated by basing it on an integer power of two samples of the time-domain signal. Samples of the DFT power spectrum computed by the computer **44** are applied serially to linear-to-logarithm conversion read-only memory **45**. The ROM **45** supplies its logarithmic samples to a digital subtractor **46** as its subtrahend input signal.

A read-only memory **47** serially generates samples of the logarithm of an ideal DFT power spectrum for the transmission channel and supplies those logarithmic samples to the subtractor **46** as its minuend input signal. The ideal DFT power spectrum for the transmission channel that is stored in the ROM **47** corresponds with the results of a lowpass filtering of the power spectrum for the PN1023 sequence as resampled to contain the same number of samples that is an integral power of two as in the resampled response to the signal that the gating circuitry **43** selects. The lowpass filtering is done with an ideal lowpass filter characteristic having a Nyquist slope roll-off that minimizes intersymbol interference.

The difference output signal from the subtractor **46** is supplied to a read-only memory **48** that stores antilogarithm look-up tables. The response of the ROM **48** is supplied to a computer **49** which computes the inverse discrete Fourier transform (I-DFT) of that response to generate a time-domain description of the transmission/reception channel system response to an impulse. This "channel impulse response" or "CIR" in the time domain is referred to as a "cepstrum", the word "cepstrum" being an anagram of the word "spectrum" descriptive of the transmission/reception channel system response in the

frequency domain. The cepstrum takes the form of a succession of pulses at time intervals indicative of the relative delays of respective multipath components and with amplitudes indicative of the relative amplitudes of those multipath components. This time-domain description is supplied to the computer **40**, which
5 generates therefrom a set of initial weighting coefficients for the adaptive filtering used to equalize the transmission/reception channel and suppress echoes.

Methods for computing the initial weighting coefficients from the cepstrum are known in the art. The weighting coefficients for the second FIR filter **35** used for suppressing longer-delayed post echoes are generated by simply scaling
10 from corresponding terms in the cepstrum. The weighting coefficients for the first FIR filter **33** can be computed by scaling from the inverse-DFT of the term-by-term complex reciprocals of the portion of the cepstrum descriptive of the pre-echoes and short post-echoes that the first FIR filter **33** is to suppress.

The set of weighting coefficients first generated after the DTV receiver is energized, or after the DTV receiver tunes to receive a different channel, is used
15 to initialize the coefficients of the adaptive filtering. Thereafter, the computer **40** adapts the weighting coefficients incrementally using decision-feedback technique. Each time a new set of weighting coefficients is generated from the ECR signal extracted from the final data segments of a new data field, the
20 computer **40** compares that set to the set of weighting coefficients as adjusted using decision-feedback technique. When the comparison indicates the set of weighting coefficients as adjusted using decision-feedback technique is in error, the adaptive filtering coefficients are re-initialized using the set of weighting coefficients most recently generated from the ECR signal.

25 Resampling the 1023-symbol-epoch portion of digitized baseband DTV signal that the gating circuitry **43** selects to the dedicated computer **44** for calculating the DFT power spectrum of **44** maps the one cycle of the PN sequence information to one cycle of DFT, so there is a seamless transition from the conclusion of the cycle to its beginning in the modular signal that theoretically
30 extends over all time. Similar sampling procedures are employed to define the

DFT power spectrum of the ideal channel response to the Nyquist-limited PN1023 sequence. These procedures cause the cycle-to-cycle aliasing of these signals in the time domain to be such that each exhibits the correct wrap-around so that the aliasing will not affect de-convolution procedures in the Nyquist-limited frequency domain. These resampling procedures are more easily performed outside real time, of course.

Alternatively, the DTV receiver can be designed so the demodulator and analog-to-digital conversion circuitry **32** supplies baseband DTV signal sampled at an integer multiple of 1024/1023 times baud rate. This clock rate simplifies DFT calculations, but complicates the design of decimation filter **36**, the interpolation filter **38** and the rest **39** of the DTV receiver.

The inventors have discerned practical designs that avoid the extensive multiplication procedures associated with the interpolative filtering for resampling the PN sequences, which designs the inventors believe to be inventive over previous designs more closely following the precepts of U. S. patent No. 5,065,242. These practical designs approximate the transmission/reception channel characteristic with sufficient precision that initial filter coefficients can be calculated for the adaptive filtering used for channel equalization and echo cancellation, which initial filter coefficients will open the eye characteristic of the DTV signal sufficiently that estimates can be generated of which multi-level data symbols have been transmitted to the DTV receiver. Decision-error feedback methods can then be used for correcting the filter coefficients for the adaptive filtering.

Designs are possible in which the PN1023 functions are extended with null samples to respective signals consisting of samples an integer power two in number, each of which extended signals has a duration equal to the same integer multiple at least two of 1024 symbol epochs. The DFTs of these extended PN1023 functions can then be differentially combined to generate the DFT of a deconvolution result. This DFT can be inverse-transformed to obtain the deconvolution result, which characterizes the transmission/reception channel.

Designs are also possible in which the PN1023 functions are extended by repetition and additional null samples to respective signals consisting of samples an integer power of two in number, each of which extended signals has a duration equal to the same integer multiple at least two of 1024 symbol epochs.

- 5 The DFTs of these extended PN1023 functions can then be differentially combined to generate the DFT of a deconvolution result. This DFT can be inverse-transformed to obtain the deconvolution result, which is the cepstrum that characterizes the transmission/reception channel.

- These approximations to deconvolution tend to have noisy measurements
10 of further-advanced pre-echoes and noisy measurements of further-delayed post-echoes. Because of the orthonormality of the PN1023 functions, practical designs for initializing the filter coefficients exist that use cross-correlation of the PN1023 functions in the DFT domain, rather than their de-convolution, better to avoid noisy measurements of further-advanced pre-echoes and noisy
15 measurements of further-delayed post-echoes. In these designs a number N of successive cycles of the 1023-symbol-epoch portion of digitized baseband DTV signal as selected to the dedicated computer **44** by the gating circuitry **43** is padded with consecutive null samples when looping it for subsequent DFT calculation. These null samples extend the successive cycles of that 1023-
20 symbol-epoch portion to generate a first signal consisting of samples an integer power of two in number, the DFT of which is computed as a first DFT. A number M of successive cycles of the Nyquist-filtered PN1023 sequence form a block of samples that is reversed in temporal order and padded with consecutive null samples to generate a second signal consisting of samples the same integer-
25 power-of-two in number, the DFT of which is computed as a second DFT. The first and second DFTs are convolved to generate a third DFT. The inverse-DFT of this third DFT is descriptive of the cross-correlation of the Nyquist-filtered PN1023 sequence as actually received with the Nyquist-filtered PN1023 sequence as known to have been transmitted. If M and N differ, the wrap-around
30 portions of the third DFT do not overlap. So, if M and N differ, the inverse-DFT

does not intermingle post-echo and pre-echo components of different cycles of repetitive PN1023 sequence that are not contiguous in time.

J. D. McDonald has investigated results obtainable from padding two successive cycles of the 1023-symbol-epoch portion of the digitized baseband DTV signal selected by the gating circuitry **43** with null samples, to extend duration of the complete signal to 2048 symbol epochs. The DFT of this modular signal was convolved with the DFT of a second signal formed by extending to 2048 symbol epochs a single cycle of Nyquist-filtered PN1023 sequence arranged in proper temporal order, the extension being made with null samples. Initial filter coefficients calculated from the result of inverse-DFT of the convolution result sufficed to open the eye characteristic of the DTV signal sufficiently to be able to generate viable estimates of which multi-level data symbols have been transmitted to the DTV receiver. Larger values of M and N will improve the accuracy of the initial filter coefficients.

FIGURE 6 shows another receiver for broadcast DTV signals capable of utilizing the preferred repetitive-PN1023 signal of FIGURES 3B, 3C, 3D, 3E, 3H, 3I, 3J and 3K. The computers **44** and **49**, the subtractor **46**, and the ROMs **45**, **47** and **48** included in the FIGURE 5 DTV receiver and connected to form apparatus for computing the cepstrum using DFT are not included in the FIGURE 6 DTV receiver. Instead, the cepstrum is generated using a PN1023 auto-correlation filtering technique.

A time-division multiplexer **50** is connected and operated so as to reproduce as its output signal either input signal received from a shift register **51** or input signal received from the demodulator and analog-to-digital conversion circuitry **32**. The multiplexer **50** selects a 1023-symbol-epoch portion of the digitized baseband DTV signal that the demodulator and analog-to-digital conversion circuitry **32** supplies with appropriate band-shaping including Nyquist-slope filtering. The selected portion of the digitized baseband DTV signal is then looped back on itself to form an extended signal to be subjected to PN1023 auto-correlation filtering. The multiplexer **50** selects this 1023-symbol-epoch portion

from the 312th and 313th data segments of each data field so as to occur after the disappearance of the longest-delayed post-echo of the data in the 310th segment, but before the appearance of the earliest pre-echo of the DFS signal in the initial data segment of the succeeding data field. This selection is analogous to the

5 selection of a 1023-symbol-epoch portion of the digitized baseband DTV signal that the gating circuitry **43** performs in the FIGURE 5 DTV receiver. The 1023-symbol-epoch portion of the digitized baseband DTV signal that the multiplexer **50** selects from the 312th and 313th data segments of each data field is reproduced in its output signal applied to the 1023-stage shift register **51** as shift

10 input signal. After the multiplexer **50** selects the 1023-symbol-epoch portion of the digitized baseband DTV signal for application to the shift register **51** as shift input signal, the shift output signal from the shift register **51** is selected by the multiplexer **50** for reproduction in its own output signal applied to the shift register **51** as shift input signal. Accordingly, after a 1023-symbol-epoch delay the shift

15 register **51** reproduces in its shift output signal the 1023-symbol-epoch portion of the digitized baseband DTV signal previously selected by the multiplexer **50**. The shift register **51** continues to reproduce that 1023-symbol-epoch portion over and over again in its shift output signal until such time a data field later that the multiplexer **50** next selects another 1023-symbol-epoch portion of the digitized

20 baseband DTV signal.

The cyclically repeating PN1023 sequence and its attendant echo information that stream from the shift register **51** as shift output signal are filtered to remove an accompanying direct component that results from the synchronous demodulation of the pilot carrier signal in the demodulator and analog-to-digital

25 conversion circuitry **32**. After the accompanying direct component is removed, the cyclically repeating PN1023 sequence and its attendant echo information are supplied as input signal to a PN1023 auto-correlation match filter **52**. The PN1023 match filter **52** responds to supply cepstrum signal to the filter-coefficient computer **40**, which generates a set of weighting coefficients for the adaptive

30 filtering therefrom. The set of weighting coefficients first generated after the DTV receiver is energized or after the DTV receiver tunes to receive a different

channel is used to initialize the coefficients of the adaptive filtering. Thereafter, the computer **40** adapts the weighting coefficients incrementally using decision-feedback technique. Each time a new set of weighting coefficients is generated from the ECR signal extracted from the final data segments of a new data field, the computer **40** compares that set to the set of weighting coefficients as adjusted using decision-feedback technique. When the comparison indicates the set of weighting coefficients as adjusted using decision-feedback technique is in error, the adaptive filtering coefficients are re-initialized using the set of weighting coefficients most recently generated from the ECR signal.

There are a number of ways to remove the direct component accompanying the shift output signal from the shift register **51**, so as to furnish only cyclically repeating PN1023 sequence and its attendant echo information as input signal to the PN1023 match filter **52**. FIGURE 6 shows the multiplexer **50** output signal applied to the shift register **51** as shift input signal also being applied as input signal to an accumulator **53** which accumulates the samples in the 1023-symbol-epoch portion of the digital baseband DTV signal the multiplexer **50** selects each data field from the demodulator and analog-to-digital conversion circuitry **32**. The shift output signal from the shift register **51** is supplied as multiplicand signal to a digital multiplier **54** for multiplication by a fixed multiplier signal equal to R times 1027, R being the number of samples per symbol epoch in the digital baseband DTV signal. Since multiplication is by a fixed multiplier, the digital multiplier **54** is best realized in read-only memory addressed by the shift output signal from the shift register **51**, there being very little latency in the generation of product signal. A digital subtractor **55** receives this product signal as its minuend input signal and receives as its subtrahend input signal the output signal from the accumulator **53**. There is a left shift **56** of binary point in the connection applying the difference output signal from the digital subtractor **55** to the PN1023 match filter **52** as its input signal.

This suppression of the pedestal component of digitized baseband DTV signal arising from synchronous detection of the pilot carrier is of particular interest, since the technique is very different from that used to suppress the

pedestal of GCR signals in NTSC analog television. The technique of pedestal-suppression used in the FIGURE 6 DTV receiver avoids the need for differentially combining oppositely poled PN sequences from successive fields to eliminate the direct pedestal component. In principle the 1023R samples in a PN1023
5 sequence are averaged to determine the direct component of those samples, which is then differentially combined with those samples before their application to the PN1023 match filter **52** as its input signal. The multiplier R is the number of samples per symbol epoch. Since it is the scaling of the echoes to the principal signal that is primarily the information of interest in echo measurement,
10 rather than the absolute levels of these signals, the pedestal-suppression filtering shown in FIGURE 6 is configured to avoid the division by 1023R that is required for straightforward averaging of the 1023R samples in a PN1023 sequence.

The accumulator **53** will have as a component of its response a term 1023R times as large as the direct component in each of the 1023R samples in
15 the one cycle of the PN1023 sequence selected by the multiplexer **50**, which direct component arises from synchronous detection of pilot carrier that ideally has a +1.25 normalized modulation level. The accumulator **53** will have as another component of its response a term arising from the fact that the PN1023 sequence has one more symbol with one of the normalized modulation levels +5
20 and -5 than with the other normalized modulation level. This other component of the accumulator **53** response will approach a level 4R times as large as the direct component in each of the 1023R samples in the one cycle of the PN1023. In the FIGURE 6 DTV receiver this other component of the accumulator **53** response is presumed to be the same polarity as the direct component that arises from
25 synchronous detection of pilot carrier. That is, the single cycle of repetitive-PN1023 sequence selected by the multiplexer **50** presumably has 512 symbols with +5 modulation level but only 511 symbols with -5 modulation level. So the total accumulator **53** response at the end of the accumulation period spanning one cycle of PN1023 sequence will approach a value 1027R times as large as
30 the direct component in each of the 1023R samples in the one cycle of that sequence. The digital subtractor **55** receives as its minuend input signal the

samples of the shift output signal from the shift register **51** response multiplied by the constant factor essentially equal to $1027R$. The digital subtractor **55** receives as its subtrahend input signal the accumulator **53** output signal having a value essentially $1027R$ times as large as the direct component in each of the $1023R$ samples in the one cycle of PN1023 sequence. The digital subtractor **55** responds to these minuend and subtrahend input signals with a difference output signal that corresponds to the shift output signal from the shift register **51** response multiplied by the constant factor essentially equal to $1027R$, but has substantially no accompanying direct pedestal term. The connection **56** shifts the binary point of this difference output signal several binary places to the left to divide it by a factor close to $1027R$. The less significant bits of each resulting quotient sample can be discarded before applying it to the PN1023 auto-correlation filter **52** as input signal thereto. Such round-off procedure reduces the bitwidth requirement of digital delay stages used in constructing the PN1023 match filter **52**.

Owing to signal transitions being affected by the limited bandwidth of the receiver, the level of the component of the accumulator **53** response caused by the PN1023 sequence presumably having 512 symbols with +5 modulation level but only 511 symbols with -5 modulation level may be slightly less than $4R$ times as large as the direct component in each of the $511R$ samples in the one cycle of the PN1023 sequence. This can be compensated for by slightly changing the constant by which the digital multiplier **54** multiplies the samples of the shift output signal from the shift register **51**.

The PN1023 auto-correlation match filter **52** is a finite-impulse-response (FIR) digital filter with kernel coefficients corresponding to the PN1023. That is, presuming the sample rate to be a multiple of the baud rate, the kernel coefficient is +1 for samples occurring during a modulation level of +5 in a particular phase of the PN1023 sequence and is -1 for samples occurring during a modulation level of -5 in that particular phase of the PN1023 sequence. Accordingly, the PN1023 auto-correlation match filter **52** can be constructed from a chain of clocked digital adders and subtractors, presuming the sample rate to be a

multiple of the baud rate. If the sample rate is not a multiple of the baud rate, the match filter will require digital multipliers in its construction. The weighting coefficients are defined by the particular phase of the PN1023 sequence subjected to raised-root-cosine lowpass filtering with roll-off at 5.38 MHz.

5 This alternative construction can also be employed even if the sample rate is a multiple of the baud rate and may provide slightly more accurate echo-location information because intersymbol interference is suppressed. However, the strong auto-correlation of a PN sequence tends to forestall problems from intersymbol interference.

10 Modification of the FIGURE 6 DTV receiver to accommodate the single cycle of repetitive-PN1023 sequence selected by the multiplexer **50** having 512 symbols with -5 modulation level but only 511 symbols with +5 modulation level is done by replacing the digital multiplier **54** having a fixed multiplier signal of 1027R with a digital multiplier having a fixed multiplier signal of 1019R.

15 The inventors currently prefer the FIGURE 6 DTV receiver and its variants over the FIGURE 5 DTV receiver and its variants. Since the FIGURE 6 DTV receiver and its variants do not require DFT computations to characterize the transmission/reception channel, these DTV receivers avoid the need for resampling the repetitive-PN-1023 sequences in order to expedite DFT
20 computations. This results in a considerable saving in computations. The repetitive-PN-sequence matched filtering employed in the FIGURE 6 DTV receiver and its variants is readily implemented with simple temporary-storage registers and tree-addition circuitry, with no need for complex digital multiplier structures.

25 FIGURE 7 shows in greater detail the rest **39** of the DTV receiver, shown as a single block in the block schematic diagrams of FIGURES 5 and 6. For the most part, the rest **39** of the DTV receiver is of conventional design.

Synchronization signal extraction circuitry **57** is connected to receive equalized digital baseband signal from the digital subtractor **34**. The sync signal

extraction circuitry **57** extracts synchronization information from the equalized digital baseband signal and supplies the synchronization information to receiver clocking and timing circuitry **58**. By way of example, the synchronization signal extraction circuitry **57** includes a narrowband bandpass filter for extracting 5.38
5 MHz component from the equalized digital baseband signal supplied from the digital subtractor **34**. The narrowband bandpass filter response is squared, and the 10.76 MHz component resulting from the squaring procedure is used as a reference for developing an automatic frequency and phase control for a master clock oscillator. This master clock oscillator (not explicitly shown in FIGURE 7) is
10 included in the receiver clocking and timing circuitry **58** for clocking the receiver operation at multiples of baud rate.

The receiver clocking and timing circuitry **58** usually includes counter circuitry for controlling receiver operation throughout each data frame. This counter circuitry (not explicitly shown in FIGURE 7) counts oscillations of the
15 master clock oscillator, and the count output signals are synchronized to the data frame by signals that the sync signal extraction circuitry **57** extracts from the equalized digital baseband signal supplied from the digital subtractor **34**. The counter circuitry typically includes a counter for counting oscillations of the master clock oscillator to generate a count descriptive of the number of symbols
20 per data segment. This counter is reset so its count is initialized at the beginning of each data segment. This resetting is done in response to circuitry for detecting the occurrence of data segment synchronization (DSS) signals, which circuitry (not explicitly shown in FIGURE 7) is included in the sync signal extraction circuitry **57**. The circuitry for detecting DSS signals can be of the type
25 described in U.S. patent No. 5,594,506 issued 14 January 1997 to J. Yang and titled "LINE SYNC DETECTOR FOR DIGITAL TELEVISION RECEIVER". The counter circuitry in the receiver clocking and timing circuitry **58** typically includes a data segment counter, which counts the DSS signals that are detected. During its normal operation the data segment counter rolls over to initial condition during
30 the initial data segment of each data field, and the data segment counter is to be reset to initial condition during the initial data segment of each data field should

rollover not occur. To implement the resetting, the sync signal extraction circuitry **57** includes a match filter (not explicitly shown in FIGURE 7) that detects the occurrence of the PN511 sequence in the initial data segment of each data field. The pulse output of the match filter to the occurrence of the PN511 sequence in the initial data segment of a data field is used to reset the data segment counter to its initial condition.

Symbol synchronizer or phase tracker **59** is connected to receive equalized digital baseband signal from the digital subtractor **34** and to supply its response to a trellis decoder **60**, which typically is of 12-phase design as described in ATSC Document A/54, Section 10.2.3.9. The trellis decoder is disabled during the data segments added to each data field for containing the repetitive-PN1023 training signal, as well as during the first data segment of each data field. The symbol synchronization or phase tracker **59** can be of the design described in ATSC Document A/54, Section 10.2.3.8, including a further decision-feedback loop for suppressing phase noise from the equalized digital baseband signal supplied to the trellis decoder **60**. When the DTV signal is not trellis-coded, the trellis decoder **60** is replaced by a suitable symbol decoder of different type, of course. For example, DTV transmissions may be 2-VSB signals without trellis coding.

The trellis decoder **60** (or alternative symbol decoder) is connected for delivering symbol decoding results to a byte assembler **61**, which assembles the symbol decoding results into 8-bit bytes for application to a convolutional de-interleaver **62**. Convolutional de-interleaver **62** reverses the convolutional interleaving introduced by the convolutional interleaver **06** in the FIGURE 4 transmitter. The convolutional de-interleaver **62** is operated somewhat differently than in an A/53 DTV receiver. The operation of the convolutional de-interleaver **62** skips over the data segments added to the data field for containing the repetitive-PN1023 training signal, as well as skipping over the first data segment.

A Reed-Solomon decoder **63** is connected to receive the de-interleaved data from the convolutional de-interleaver **62**. The Reed-Solomon decoder **63**

responds to the Reed-Solomon forward-error-correction coding contained in that de-interleaved data to correct burst errors of less than a specified number of bytes and to detect errors of longer duration than be corrected. Error detection and correction is done on that de-interleaved data before its application to a data de-randomizer **64** so that the data de-randomizer **64** is better able to reproduce the packetized data supplied from the packet assembler **02** to the data randomizer **03** in the FIGURE 4 transmitter. The data de-randomizer **64** exclusive-ORs the error-corrected de-interleaved data with a prescribed de-randomizing signal data to reproduce packetized data supplied to a packet sorter **65**, which sorts packets responsive to their header information.

The packet sorter **65** is also called the "transport-stream de-multiplexer". The packet sorter **65** selects packets containing compressed video information for application to MPEG-2 video decompression circuitry **66** and selects packets containing compressed audio information for application to AC-3 audio decompression circuitry **67**. In a complete DTV receiver system the MPEG-2 video decompression circuitry **66** forwards de-compressed video signals to the DTV receiver display system **68**, and the AC-3 audio decompression circuitry **67** forwards de-compressed audio signals to the DTV receiver sound system **69**.

Besides the trellis decoder **60** and the convolutional de-interleaver **62** having to be clocked somewhat differently to confine their operations to the 2nd through 313th data segments of each data field, there is a further way in which the operation of the rest **39** of the DTV receiver is affected to some extent. During the 2nd through 313th data segments estimates of the symbols transmitted to the DTV receiver, which the filter-coefficients computer **40** uses for adapting the coefficients of the FIR filters **33** and **35** on a tracking basis, are extracted from symbol decoding results generated by the trellis decoder **60** or by another symbol decoder. Customarily, the estimates of the first 700 symbols following the DSS sequence in the first data segment are not extracted from symbol decoding results from the trellis decoder **60** or from another symbol decoder, but instead are read from read-only memory within the computer **40**. The higher confidence level in the estimates supplied from ROM facilitates reduction of

tracking error. The addressing for this ROM is generated within the receiver clocking and timing circuitry **58**. When extra data segments containing repetitive-PN1023 training signal are appended to each data field, the addressable locations in the ROM can be increased for storing high-confidence estimates of the symbols in these extra data segments. The receiver clocking and timing circuitry **58** is modified for generating the additional addressing for the increased ROM.

The foregoing specification describes, with reference to FIGURES 5 and 6 of the drawing, DTV receivers in which the adaptive filter provides for channel equalization and echo cancellation at baseband using fractional equalization of real signals. Other DTV receivers, which embody the invention in others of its aspects, use adaptive filters providing equalization of complex signals. Such equalization can be easily carried out using baud-rate samples; there is less need for oversampling if equalization is performed on complex signals. In still other DTV receivers, which can be modified for embodying the invention in others of its aspects, I-F DTV signal is digitized for application to an adaptive filter that provides for channel equalization and echo cancellation in the I-F passband. The adaptive filter response is then demodulated to obtain baseband signals for application to the trellis decoding apparatus. Through acquaintance with this specification and its drawing, one skilled in the art of equalizer design will be enabled to adapt the invention for use in many known adaptive filtering schemes used for channel equalization and echo suppression.

The operational procedures of the computer **40** in the FIGURE 5 or FIGURE 6 DTV receiver can take a variety of forms known in the art. The cepstrum provided to the computer **40** from the computer **49** in the FIGURE 5 DTV receiver and from the PN1023 auto-correlation filter **52** in the FIGURE 6 DTV receiver will be used differently in these various ways of operating the computer **40**. The cepstrum of the required time-domain filter that the computer **49** in the FIGURE 5 DTV receiver or the PN1023 auto-correlation filter **52** in the FIGURE 6 DTV receiver supplies is a "snapshot" of what the effective overall kernel of the adaptive filter should be at the beginning of the "motion picture" of

the change in the kernel that is to take place when tracking dynamic multipath variation. This provides a basis for greatly simplifying the tasks to be performed by the computer 40.

This is especially so because much of dynamic multipath distortion is
5 continuous in nature, with very little change in transmission/reception channel characteristic occurring from each symbol epoch to the next. Accordingly, the initial adaptive filtering coefficients determined from the ECR signal afford a basis from which tracking procedures based on decision feedback methods do not have to hunt much for convergence before beginning the tracking of the changes
10 in channel characteristic resulting from incrementally changing multipath distortion. One exception to dynamic multipath distortion being continuous in nature is the well-known suddenly-revealed-ray exception in which a path closed off to reception is abruptly opened for reception. Another exception is the well-known suddenly-masked-ray exception in which a path open for reception is abruptly
15 closed to reception. Tracking of dynamic multipath by the adaptive filtering is disrupted when either of these exceptions occurs, and rapid re-initialization of the adaptive filtering coefficients becomes the immediate concern. The determination of the initial adaptive filtering coefficients directly from the ECR signal without relying on decision feedback assures that reception can be
20 restored within less than about 25 milliseconds whenever either one of these exceptions occurs.

There are a number of methods for determining whether such an exception remains uncorrected for at the end of a data field. One method compares the weighting coefficients of the adaptive filtering at the conclusion of
25 the data field, as they have been adjusted by decision feedback, with the weighting coefficients of the adaptive filtering as calculated from the repetitive-PN1023 sequence. Substantial discrepancies between the two sets of coefficients is evidence that dynamic multipath distortion exhibited a severe discontinuity in the previous data field, which has not been corrected for, and that
30 the adaptive filtering preferably should proceed with the weighting coefficients calculated from the repetitive-PN1023 sequence. In another method for

determining whether dynamic multipath distortion exhibited a severe discontinuity that has not been corrected for at the end of a data field, the magnitudes of decision-feedback error samples near the conclusion of each data field are measured, and the measurements are averaged. A high average is evidence
5 that dynamic multipath distortion exhibited a severe discontinuity in the previous data field, which has not been corrected for, and that the adaptive filtering preferably should proceed with the weighting coefficients calculated from the repetitive-PN1023 sequence.

In many of the various ways of operating the computer **40**, an initial
10 consideration in evaluating the cepstrum is determining what will be considered the principal or "cursor" component of the received DTV signal when multipath reception obtains. This cursor component is used as a reference for determining whether each other component of the received DTV signal when multipath
15 reception obtains, as differentially delayed with respect to the cursor component, is to be considered pre-echo or a post-echo. Each later-arriving component of the received DTV signal is considered to be a "post-echo", and its arrival time is measured relative to that of this cursor component, being typically measured as a
20 positive delay (or alternatively as a negative advance). Each earlier-arriving component of the received DTV signal is considered as a "pre-echo", and its arrival time is measured relative to that of this cursor component, being typically measured as a negative delay (or alternatively as a positive advance).

In some operational procedures for the computer **40**, the largest of the differentially-delayed components of the received DTV signal is chosen as the cursor component. This procedure admits the existence of pre-echoes of
25 substantial energy preceding the cursor component. The existence of pre-echoes of substantial energy increases the kernel width needed in the FIR filter **33** to accommodate the most advanced of these pre-echoes. Furthermore, the suppression of echoes in the feed-forward FIR filter **33** is accomplished by weighted summation of samples of signal that have not been subjected to echo-
30 suppression. This contrasts with the suppression of echoes by the IIR filter including the feedback FIR filter **35**, which is accomplished by weighted

summation of samples of signal that have been subjected to echo-suppression. The suppression of echoes by the IIR filter suppresses the echo components without introducing additional echo components. The suppression of echoes by the feed-forward FIR filter **33** results in the introduction of echo repeat

5 components with twice the differential delay respective to the cursor component of signal, which echo repeat components are reduced in amplitude compared to the original echo components suppressed in the feed-forward FIR filter **33** response. The reduction in amplitude of these singly-repeated echo repeat components is substantial for a transmission/reception channel in which the

10 cursor component of the cepstrum is substantially larger than the other components. The reduction is usually sufficient that these echo repeat components are lost in the digital signal quantization. For a transmission/reception channel in which the cursor component of the cepstrum is not substantially larger than the other components, however, the singly-repeated

15 echo repeat components have substantial amplitude, and even multiply-repeated echo repeat components will in some instances have substantial amplitude.

The echo repeat components that are post-echoes can be cancelled by the IIR filter cascaded with the feed-forward FIR filter **33** when the decision-feedback method takes over. So the FIR filter **33** kernel need not extend enough

20 in the time-lag direction to provide capability for suppressing post-echo repeats that can be cancelled in the IIR filter. The IIR filter has no capability for canceling or suppressing echo repeat components that are pre-echoes, however, so the FIR filter **33** kernel width needs to extend far enough in the time-advance direction to provide capability for reducing the amplitudes of all repeats of these

25 pre-echoes to insignificant values when the decision-feedback method takes over, so that these pre-echo repeats will be lost in the digital signal quantization.

In alternative operational procedures for the computer **40**, one of the earlier received differentially-delayed DTV signals having significant energy is chosen as the cursor component. This procedure can eliminate pre-echoes of

30 substantial energy preceding the cursor DTV signal and so reduce the kernel width needed in the FIR filter **33**. However, unless the received DTV signal that

is chosen as cursor component is substantially as strong as the strongest received DTV signal component, the C/N of the adaptive filtering response is substantially lowered from what it would be were the strongest received DTV signal component chosen as cursor component. It is generally preferable that the DTV receiver be designed to choose the strongest received DTV signal component as cursor component when the received DTV signals are accompanied by substantial noise. The availability of the cepstrum generated from one cycle of the repetitive-PN1023 sequence provides information that can provide a basis for deciding which of the received DTV signal components is best chosen as cursor component.

It is desirable to avoid changing the cursor component during a data field because of the latency of samples within the adaptive filtering. The availability of the cepstrum of the time-domain filter at the conclusion of each DTV data field facilitates the computer **40** selecting one of the differentially-delayed components of the received DTV signal to be the cursor component for the entirety of the next data field. Under certain reception conditions a component chosen as cursor component may substantially decline in energy during a data field, which makes it desirable to select a component with greater energy as cursor component for the next data field. Such a substantial decline in energy is signaled by the decision-feedback procedure making large increase(s) in the filter coefficient(s) associated with the cursor component. The digital multipliers that the adaptive filters **33** and **35** use for weighting differentially delayed DTV signals must have sufficient dynamic range for accommodating weighting coefficients with amplitudes several times unity. Generally, it is preferable that, so long as the decision-feedback procedure exhibits reasonably small tracking errors, the computer **40** maintains the same cursor component from one data field to the next. So, the repetitive-PN1023 sequence is not used for generating a complete revision of the adaptive filter coefficients at the beginning of a data field provided that the decision-feedback procedure has been exhibiting reasonably small tracking errors. However, if the decision-feedback procedure has been exhibiting reasonably small tracking errors, it is attractive to base estimates of transmitted

signal during the final three data segments of each data field on the repetitive-PN1023 sequence as stored at the receiver, rather than from received DTV signal. This increases the confidence factor of the corrections the decision-feedback procedure generates during the repetitive-PN1023 sequence in the
5 final three data segments of each data field, as well as during the PN511 sequence and the triple-PN63 sequence in the initial data segment of each data field. The higher confidence factor facilitates greater gain in the incremental corrections made to adaptive filtering coefficients during these times, improving tracking accuracy.

10 Many designs for a DTV receiver embodying the invention in certain of its aspects will provide for temporal buffering between the various procedures for adapting the adaptive filtering used for channel-equalization and echo cancellation. The means providing for this temporal buffering are not explicitly shown in FIGURES 5 and 6, but are typically provided for by digital random-
15 access memory (RAM). Of especial interest is a particular use of digital memory configured to introduce first-in-first-out (FIFO) buffering delay into the application of input signal supplied from the demodulator and ADC circuitry **32** to the feed-forward FIR filter **33**. The FIFO buffering is made long enough to allow the time required for processing the repetitive-PN1023 sequence extracted from the
20 circuitry **32** output signal, in order to generate initial weighting coefficients of the FIR filters **33** and **35**, to transpire just before the 311th data segment of the previous data field begins to be supplied from the interpolation filter **38** to the subtractor **41**. Then, instead of the decision-feedback error signal being generated as the difference of the adaptive filtering response as supplied from
25 the compensatory delay **41** from the response of the interpolation filter **38**, as implied in FIGURES 5 and 6, decision-feedback error signal is generated as the difference of the adaptive filtering response as supplied from the compensatory delay **41** from the Nyquist-filter response to the repetitive-PN1023 sequence, ensuing PN511 sequence and ensuing PN63 sequence(s) as known *a priori* at
30 the DTV receiver. The high confidence factor of this alternative decision-feedback error signal facilitates greater gain in the incremental corrections made

to adaptive filtering coefficients during these times, improving the speed of the decision-feedback adaptation in suppressing any coefficient error remnant after initialization.

Though not explicitly shown in FIGURES 5 and 6, in some designs for a DTV receiver embodying the invention in certain of its aspects there will be digital memory for buffering the application of incremental updates of the weighting coefficients of the FIR filters **33** and **35** to the coefficient registers of these filters, which incremental updates are generated by decision-feedback procedures. Such buffer memory facilitates the reversal-of-real-time calculations of those updates by a block-LMS algorithm, for example.

Though not explicitly shown in FIGURES 5 and 6, in some DTV receiver designs the means for temporal buffering will also include digital memory configured to introduce FIFO buffering delay into the application of difference output signal from the subtractor **34** to the rest **39** of the DTV receiver. Designs including such FIFO digital memory, the FIFO digital memory for controlling the application of input signal supplied from the circuitry **32** to the feed-forward FIR filter **33**, and digital buffer memory for controlling the application of incremental updates to the weighting coefficients of the FIR filters **33** and **35** permit the adaptive filtering to be operated asynchronously with respect to the baud rate of received signal. For example, it is desirable to permit data-directed stochastic procedures for adapting the coefficients of the filters **33** and **35** to be clocked at increased rates if re-computations of weighting coefficients are necessitated when attempting to track dynamic echo components. The rate data is advanced through the adaptive filtering *per se* can be varied, even halted briefly at times, with the FIFO memories preceeding and succeeding the adaptive filtering *per se* generating an overall system function with uniform latency.

Rather than having the structure shown in FIGURES 5 and 6, the adaptive filtering could be constructed to use a single FIR filter for channel equalization and echo cancellation. By way of example, such an alternative is described in U.S. patent No. 5,648,987 issued 15 July 1997 to J. Yang, C. B. Patel, T. Liu & A.

L. R. Limberg, entitled "RAPID-UPDATE ADAPTIVE CHANNEL-EQUALIZATION FILTERING FOR DIGITAL RADIO RECEIVERS, SUCH AS HDTV RECEIVERS".

Yang *et alii* use another FIR filter to implement a block-LMS algorithm for updating the coefficients of the adaptive FIR filter used for channel equalization

5 and echo cancellation. If a single adaptive FIR filter were used for channel equalization and echo cancellation, the kernel of that adaptive FIR filter at the time the "snapshot" is extracted could be approximated by the following

procedure from the cepstrum of the required time-domain filter that the computer

49 in the FIGURE 5 DTV receiver or the PN1023 auto-correlation filter 52 in the

10 FIGURE 6 DTV receiver. All components of the cepstrum except that selected to be the "cursor", occurring at the time that the principal multipath component of the DTV signal is considered to be received, would have their polarity changed with respect to the cursor. This approximation method works reasonably

satisfactorily for a Ricean transmission/reception channel, for which the cursor

15 component of the cepstrum is substantially larger than the other components and for which echoes exhibit short differential delay from the cursor component as compared to the kernel width of the FIR filter. However, this approximation

method is inaccurate when several components have energy that is several percent of the energy of the cursor component. If the adaptive filtering is to

20 correct for such a transmission/reception channel, the filter characteristic that convolves with the cepstrum to result in a Nyquist channel response is better computed by more exact means. The adaptive filtering weighting coefficients are normalized, so the dynamic range of the adaptive filtering response is suitable for input signal to the quantizer 37.

25 Using a single FIR filter for channel equalization and cancellation of all echoes including the longer-delayed post-echoes is not preferred actual practice. The transmission/reception channel is theoretically modeled as a FIR filter with different weighting coefficients for the different propagation paths having different respective delays. In actual practice, this model is also correct under static

30 multipath reception conditions. Equalization of the channel with regard to post-echoes can be exact if the adaptive filter has overall an infinite impulse response

— i. e., a time-domain response with a very large number of coefficients lagging in time. The response of a single FIR filter used for channel equalization and cancellation of all echoes including the longer-delayed post-echoes tends to have a substantially smaller number of coefficients lagging in time, so the cancellation of the longer-delayed post-echoes is not optimal. This tendency arises from the practical design imperative to keep the latent delay through the single FIR filter no more than a few times the longest delayed post-echoes with significant energy. Accordingly, the exact system function for equalization of the channel with regard to post-echoes can only be approximated in a single-FIR-filter design, even supposing the filter coefficients to be subsequently adapted by data-directed methods. The approximation procedure suppresses echoes, but undesirably generates repeats of the echoes. These repeats are attenuated relative to the suppressed echoes and exhibit differential delays relative to a cursor component of received DTV signal that are integer multiples of the suppressed echoes. Therefore, a larger number of non-zero weighting coefficients and therefore an undesirably increased number of digital multiplications are required in the single-FIR-filter design, as compared to a design using an IIR filter. Not only do more non-zero digital multiplications require more die area in an integrated-circuit design implementing them in hardware; they undesirably increase the effects on quantization noise and stochastic jitter. Accordingly, an adaptive filtering structure including an IIR section — e. g., of the type depicted in FIGURES 5 and 6 — is preferable.

In the adaptive filtering structure of either FIGURE 5 or 6, the kernel of the FIR filter **33** comprises a weighting coefficient at the "cursor" position corresponding to the time that the principal multipath component of the DTV signal is considered to be received. The filter **33** kernel further comprises a subset of coefficients corresponding to the portion of the cepstrum of the required time-domain filter preceding the "cursor" time that the principal multipath component of the DTV signal is received. The filter **33** kernel further comprises a subset of coefficients corresponding to the portion of the cepstrum that succeeds the "cursor" time by less delay than the minimum delay possible in the IIR filter

containing the FIR filter **35** in feedback loop. DTV receiver designs are known that provide crossovers between the weighting coefficients of the feed-forward FIR filter **33** and the weighting coefficients in the feedback FIR filter **35** of the IIR filter cascaded after the filter **33**. A rapid approximation method that works

5 satisfactorily for a Ricean transmission/reception channel in which the cursor component of the cepstrum is substantially larger than the other components, generates the filter **33** kernel from a corresponding portion of the cepstrum by changing the polarity of all components of the cepstrum except the cursor component. The filter **35** kernel is generated from the longer-delayed portion of

10 the cepstrum without polarity change. This approximation method is inaccurate when several components have energy that is several percent of the energy of the cursor component. If the adaptive filtering is to correct for such a transmission/reception channel, the filter characteristic that convolves with the cepstrum to result in a Nyquist channel response must be computed by more

15 exact means. The adaptive filtering weighting coefficients are normalized, so the dynamic range of the adaptive filtering response is suitable for input signal to the quantizer **37**.

More accurate computation of the weighting coefficients of the adaptive filtering proceeds from the observation that the time-domain response of the

20 complete adaptive filtering structure should correspond to the cepstrum supplied by the computer **49** in the FIGURE 5 DTV receiver or by the PN1023 auto-correlation filter **52** in the FIGURE 6 DTV receiver. The time-domain response of the complete adaptive filtering structure results from the convolution of the time-domain responses of the FIR filter **33** and of the subsequent IIR filter containing

25 the FIR filter **35** in feedback loop. As part of the DTV receiver design process the adaptive filtering system characteristic that convolves with any cepstrum of specified length to result in a Nyquist channel response for the adaptive filter structure can be computed in general terms, using Z-transform polynomials. The algebraic equations resulting from such computations can be stored in the

30 filter-coefficient computer **40** in the DTV receiver, for use in calculating adaptive filtering coefficients from the specific cepstrum supplied by the computer **49** in

the FIGURE 5 DTV receiver or by the PN1023 auto-correlation filter **52** in the FIGURE 6 DTV receiver. These algebraic equations define the adaptive filtering weighting coefficients in terms of the cepstrum values. The sub-programs employing these algebraic equations may also be employed in programs for
5 implementing the decision-directed procedures for tracking dynamic multipath distortion.

In the various ways of operating the computer **40**, another important consideration in evaluating the cepstrum is determining how the gain of the adaptive filter is to be related to the energies of the component terms of the cepstrum. A normalization of the weighting coefficients generated from the
10 cepstrum is so that the gain of the adaptive filter for principal DTV signal is always substantially the same no matter how its weighting coefficients are computed from the repetitive-PN1023-sequence ECR signal. The takeover of the tracking of multipath reception conditions by the decision-feedback
15 procedures will not be smooth if immediately after the take-over the quantizer **37** is called upon to make substantial automatic adjustment of the decision levels used for quantizing its input signal to generate estimates of transmitted symbols. There is apt to be error in the estimates the quantizer **37** makes while those decision levels are being adjusted, and the decision-feedback procedures
20 depend on these estimates being accurate most of the time in order to adjust accurately the weighting coefficients of the adaptive filtering. Normalization is done respective to the component of the cepstrum selected to be the cursor component, since this component is to be the only one that survives in the adaptive filtering response. In order that the C/N of the adaptive filtering
25 response supplied to the quantizer **37** is substantially as good as it can be, the cursor component should be one of the higher energy components of the cepstrum, if not the highest energy one. In the FIGURE 5 DTV receiver normalization is automatic providing that the DFT stored in the ROM **47** is that of a Nyquist-filtered PN1023 sequence of the correct "gain" respective to input
30 signal for the quantizer **37**.

Normalization is quite simple in the FIGURE 6 DTV receiver, too. The cursor component is known to be the sum of 1023 symbol epochs of signal modulated with a standardized-amplitude modulation signal, so a reduction in gain of each cepstrum component by a factor of 1023 will reduce the cursor component to a unity-gain coefficient. These divisions could be closely approximated by shifting the binary point of each cepstrum component ten bit places in the direction of reducing the significance of the component. In practice, the ten-bit-place binary point shift may be taken into account elsewhere in the system.

FIGURE 8A shows the cyclically repeating cepstrum of a signal received under multipath reception conditions, as that cepstrum is determined by the computer **49** in the FIGURE 5 receiver portion or by the cyclic PN713 match filter **52** in the FIGURE 6 receiver portion. The component **70** in each cycle is generated in response to the principal signal. The component **71** that precedes the component **70** in each cycle is generated in response to a pre-echo advanced by less than 47.5 microseconds, and the component **72** that succeeds the component **70** in each cycle is generated in response to a post-echo delayed by less than 47.5 microseconds.

The component **73** in each cycle is generated in response to a post-echo delayed by more than 47.5 microseconds, but less than 95 microseconds. The component **73**, although generated in response to a post-echo precedes the component **70** in each cycle, owing to the wrap-around of DFT in the FIGURE 5 receiver portion, or owing to the wrap-around of the cyclic PN713 match filter **52** in the FIGURE 6 receiver portion. Unless the component **73** precedes the component **70** in each cycle sufficiently that it is known to be outside the range for pre-echoes, there is the possibility of it being mistaken for a pre-echo.

The component **74** in each cycle is generated in response to a post-echo delayed by more than 95 microseconds. Owing to the wrap-around of DFT in the FIGURE 5 receiver portion, or owing to the wrap-around of the cyclic PN713 match filter **52** in the FIGURE 6 receiver portion, the component **74** is apt to be

confused with a post-echo with 95 microseconds less delay respective to the principal signal.

A DTV receiver can be designed presuming that post-echoes longer than 64 microseconds never have sufficient strength to cause data slicing errors so frequently that the error-correcting capability of the receiver is overwhelmed, and presuming that any component of the cepstrum that precedes the principal signal by no more 30 microseconds is attributable to a pre-echo. Such DTV receivers or minor variants thereof should work satisfactorily at most reception sites. If exceptionally long-delayed post-echoes are to be better distinguished from pre-echoes and from much less delayed post-echoes, cepstrum generated in the receiver portion of FIGURE 5 or of FIGURE 6 must be further analyzed, which further analysis can be performed using apparatus as described *infra* with reference to FIGURE 9 of the drawing.

The filter coefficient computer **40** can start with a cyclically repeating cepstrum of the type shown in FIGURE 8A and process it to generate an extended cepstrum in which many of the temporal aliases and repeats are suppressed. FIGURE 8B shows the time-domain response of an initial step in such processing of the FIGURE 8A cyclically repeating cepstrum, in which initial step the repeats of the component **70** generated in response to the principal signal are suppressed. FIGURE 8C shows an intermediate step in the processing, in which intermediate step the wrap-arounds of the pre-echoes are suppressed. FIGURE 8D shows a final step in the processing, in which final step the wrap-arounds of the post-echoes are suppressed. The intermediate and final processing steps are described *infra* in more detail.

FIGURE 9 shows apparatus that can be used for further analyzing the cepstrum of the DTV signal as received and demodulated, for implementing the intermediate and final processing steps that generate the time-domain responses of FIGURES 8C and 8D. The input signal to the FIGURE 9 apparatus is demodulated real-only baseband DTV signal from the demodulator and analog-to-digital conversion circuitry **32** of the FIGURE 5 or FIGURE 6 receiver portion,

supplied as input signal to a direct-component suppression filter **75**. The filter **75** may, for example, be of a type that generates its response by subtracting a many-symbol-epochs average of the real-only baseband DTV signal from itself. Alternatively, by way of further example, the filter **75** may be of a type that
5 performs a digital differentiation on the real-only baseband DTV signal and then performs a digital integration on the digitally differentiated real-only baseband DTV signal to recover the real-only baseband DTV signal without accompanying direct component.

A digital filter **76** is connected to receive, as its input signal, the response
10 of the direct-component suppression filter **75**. The digital filter **76** has a kernel corresponding to the final 1023 symbols of the repetitive-PN1023 sequence used as training signal for the adaptive filtering used for channel equalization and echo suppression. The digital filter **76** functions as an auto-correlation match filter for the final-phase PN1023 sequence beginning the repetitive-PN1023 sequence
15 and generates a response that contains a repeated cepstrum of the reception channel. The response of the digital filter **76** is applied without delay as subtrahend input signal to a digital subtractor **77** and as input signal to a digital delay line **78** that responds to its input signal with 1023 symbol epochs delay. The response of the digital delay line **78** is applied without delay as minuend
20 input signal to the digital subtractor **77**. The subtractor **77** and the delay line **78** form a comb filter that responds to the repeated cepstrum of the reception channel to generate a cepstrum of the reception channel preceded some time earlier by the negative of that cepstrum. The later-in-time cepstrum in the digital subtractor **77** difference signal is written into an extended-range cepstrum
25 register **79** for temporary storage. The filter-coefficient computer **40** is connected for reading the contents of the extended-range cepstrum register **79** and for correcting those contents. The register **79** contents are overwritten when the repetitive-PN1023-sequence training signal next occurs.

A digital filter **80** is connected to receive, as its input signal, the response
30 of the direct-component suppression filter **75**. The digital filter **80** has a kernel corresponding to the initial 1023 symbols of the repetitive-PN1023 sequence

used as training signal for the adaptive filtering used for channel equalization and echo suppression. The digital filter **80** functions as an auto-correlation match filter for the initial-phase PN1023 sequence concluding the repetitive-PN1023 sequence and generates a response that contains a repeated cepstrum of the reception channel. The response of the digital filter **80** is applied without delay as minuend input signal to a digital subtractor **81** and as input signal to a digital delay line **82** that responds to its input signal with 1023 symbol epochs delay. The response of the digital delay line **82** is applied without delay as subtrahend input signal to the digital subtractor **81**. The subtractor **81** and the delay line **82** form a comb filter that responds to the repeated cepstrum of the reception channel to generate a cepstrum of the reception channel succeeded some time later by the negative of that cepstrum. The earlier-in-time cepstrum in the digital subtractor **81** difference signal is written into an extended-range cepstrum register **83** for temporary storage. The filter-coefficient computer **40** is connected for reading the contents of the extended-range cepstrum register **83** and for correcting those contents. The register **83** contents are overwritten when the repetitive-PN1023-sequence training signal next occurs.

FIGURES 10A, 10B, 10C, 10D, 10E and 10D show time-domain responses at various connections in the FIGURE 9 apparatus in the time interval when repetitive-PN1023 sequence training signal occurs. FIGURES 10A, 10B and 10C show the auto-correlation match filter **76** response, that response as delayed 1023 symbols by the digital delay line **78**, and the difference between these responses that the digital subtractor **77** supplies as its output signal. FIGURES 10D, 10E and 10F show the auto-correlation match filter **80** response, that response as delayed 1023 symbols by the digital delay line **82**, and the difference between these responses that the digital subtractor **81** supplies as its output signal.

The components **71'** in the FIGURE 10A time-domain response of the PN1023 match filter **76** are cyclically generated in response to the current phasing of the pre-echo of the repetitive-PN1023 sequence corresponding to that of the initial 1023 symbols of the repetitive-PN1023 sequence. The components

72'in the FIGURE 10A time-domain response are cyclically generated in response to the current phasing of the least-delayed post-echo of the repetitive-PN1023 sequence corresponding to that of the initial 1023 symbols of the repetitive-PN1023 sequence. The components **73**'in the FIGURE 10A time-domain response are cyclically generated in response to the current phasing of the post-echo of the repetitive-PN1023 sequence delayed more than 47.5 microseconds, but less than 95 microseconds, being in correspondence with the phasing of the initial 1023 symbols of the repetitive-PN1023 sequence. The components **74**'in the FIGURE 10A time-domain response are cyclically generated in response to the current phasing of the post-echo of the repetitive PN1023 sequence delayed more than 95 microseconds being in correspondence with the phasing of the final 1023 symbols of the repetitive-PN1023 sequence.

FIGURE 10A shows a clutter component **84**. A portion of this clutter component **84** arises from the PN1023 match filter **76** response to data preceding the repetitive-PN1023 sequence and to its echoes, which portion of the clutter component **84** cannot be predicted in the receiver. Another portion of this clutter component **84** arises from the non-cyclic PN1023 match filter **76** response exhibiting edge effects at the beginning of the repetitive-PN1023 sequence, which other portion of the clutter component **84** can be predicted in the receiver.

FIGURE 10A shows another clutter component **85** arising from the non-cyclic PN1023 match filter **76** response to the DFS signal succeeding the repetitive-PN1023 sequence and to its echoes. The initial few hundred symbol epochs of clutter component **85** can in most part be predicted in the receiver. The edge effects at the conclusion of the repetitive-PN1023 sequence that the PN1023 match filter **76** response exhibits are readily predictable. The PN1023 match filter **76** response to the first 700 symbol epochs of DFS signal succeeding the repetitive-PN1023 sequence is also readily predictable. These readily predictable components of PN1023 match filter **76** response can be compensated for by *a priori* knowledge extracted from read-only memory in the computer **40**. The PN1023 match filter **76** response to the echoes of the first 700

symbol epochs of DFS signal succeeding the repetitive-PN1023 sequence is not as easily predictable.

The ordinate scale for the clutter components **84** and **85** is expanded in FIGURES 10A, 10B and 10C respective to the principal responses **70'** for sake of illustration. The echo components **71'**, **72'**, **73'** and **74'** are also somewhat larger in amplitude respective to the principal responses **70'** than is the case for a good-quality transmission channel to the receiver. The PN1023 match filter **76** has an auto-correlation function with 60 dB gain against phases of PN1023 sequence other than the final phase and with 30 dB gain against non-PN1023 signal components.

FIGURE 10B shows the digital subtractor **77** minuend signal that the digital delay line **78** supplies in response to the digital subtractor **77** subtrahend input signal as delayed by one cycle of the repetitive-PN1023 sequence — i.e., by 1023 symbol epochs.

FIGURE 10C shows the difference output signal supplied from the digital subtractor **77**. Note that in the difference output signal supplied from the digital subtractor **77** the cepstrum of the final cycle of PN1023 sequence from the minuend signal is separated from the cepstrum of any preceding PN1023 sequence and is not overlapped by components of clutter component **84**. The register **79** temporarily stores this separated cepstrum of the final cycle of PN1023 sequence from the minuend signal and is connected so its contents are available to the filter-coefficient computer **40**. As noted previously, the filter-coefficient computer **40** can compensate for the readily predictable components of clutter component **85** using a *priori* knowledge extracted from read-only memory. Presuming such processing is performed, the responses to pre-echoes in the extended-range cepstrum temporarily stored in the register **79** are contaminated very little by other time-domain response components. Even the responses to post-echoes up to 64 microseconds or so in the extended-range cepstrum are not contaminated very much by other time-domain response components.

The filter-coefficient computer **40** can then separate the time-domain response to pre-echoes to be used in further processing the cyclically repeating cepstrum as modified per FIGURE 8B. The separated time-domain response to pre-echoes can be correlated with a corresponding portion of the cyclically
5 repeating cepstrum. The correlation procedures are used to eliminate repeats of responses to pre-echoes and to eliminate aliases of post-echoes that appear as pre-echoes occurring at times when the separated time-domain response to pre-echoes does not exhibit substantial energy.

FIGURE 8C shows the result of this further pruning of the cyclically
10 repeating cepstrum. Valid pre-echoes remain as the only components preceding the remnant response to the principal received component **70** in the modified cepstrum of FIGURE 8C. The FIGURE 8C modifications of the cepstrum are by way of eliminating or reducing temporal components that arose from a cyclic cepstrum based on a PN1023 sequence free from contaminants arising from
15 edge effects, data preceding the repetitive-PN1023 sequence, or DFS signal succeeding the repetitive-PN1023 sequence. Since the FIGURE 8C modifications are the results of a pruning procedure, such contaminants in the extended-range cepstrum stored in the register **79** are not carried forward in appreciable degree into the FIGURE 8C modifications of the cyclically repeating
20 cepstrum.

The filter-coefficient computer **40** could then use the time-domain response to post-echoes up to 64 microseconds or so as a basis for further pruning the cyclically repeating cepstrum pruned per FIGURE 8C. That is, the separated time-domain response to these post-echoes could be correlated with
25 the corresponding portion of the cyclically repeating cepstrum. The correlation procedures would then be used to eliminate repeats of responses to post-echoes and to eliminate aliases of post-echoes delayed more than 95 microseconds that appear as less-delayed post-echoes. FIGURE 8D shows the result of these still further prunings of the cyclically repeating cepstrum.

The pruning of the cyclically repeating cepstrum to eliminate repeats of responses to post-echoes and to eliminate aliases of post-echoes delayed more than 95 microseconds can proceed based on an alternative method for extracting the extended-range cepstrum. This alternative method can reduce the
5 contamination of the responses to longer delayed post-echoes in an extended-range cepstrum, as caused by other time-domain response components.

FIGURE 10D shows the time-domain response of auto-correlation digital filter **80** as applied to a digital delay line **82** as input signal thereto and as applied to a digital subtractor **81** as its minuend input signal. The components **70''** in the
10 FIGURE 10D time-domain response are cyclically generated in response to the current phasing of the repetitive PN1023 sequence corresponding to that of the initial 1023 symbols of the repetitive-PN1023 sequence. The components **71''** in the FIGURE 10D time-domain response are cyclically generated in response to the current phasing of the pre-echo of the repetitive PN1023 sequence
15 corresponding to that of the initial 1023 symbols of the repetitive-PN1023 sequence. The components **72''** in the FIGURE 10D time-domain response are cyclically generated in response to the current phasing of the least-delayed post-echo of the repetitive PN1023 sequence corresponding to that of the initial 1023 symbols of the repetitive-PN1023 sequence. The components **73''** in the
20 FIGURE 10D time-domain response are cyclically generated in response to the current phasing of the post-echo of the repetitive-PN1023 sequence delayed more than 47.5 microseconds, but less than 95 microseconds, being in correspondence with the phasing of the initial 1023 symbols of the repetitive-PN1023 sequence. The components **74''** in the FIGURE 10D time-domain
25 response are cyclically generated in response to the current phasing of the post-echo of the repetitive PN1023 sequence delayed more than 95 microseconds being in correspondence with the phasing of the initial 1023 symbols of the repetitive-PN1023 sequence.

FIGURE 10D shows a clutter component **86**. A portion of this clutter
30 component **86** arises from the PN1023 match filter **80** response to data preceding the repetitive-PN1023 sequence and to its echoes, which portion of

the clutter component **86** cannot be predicted in the receiver. Another portion of this clutter component **86** arises from the non-cyclic PN1023 match filter **80** response exhibiting edge effects at the beginning of the repetitive-PN1023 sequence, which other portion of the clutter component **86** can be predicted in the receiver. This other portion of the clutter component **86** due to edge-effects does not affect the post-echoes of the initial 1023 symbols of the repetitive-PN1023 sequence, which will be of principal concern when analysis of the digital subtractor **81** difference output signal proceeds to conclusion.

FIGURE 10D shows a clutter component **87** arising from the PN1023 match filter **80** response to the DFS signal succeeding the repetitive-PN1023 sequence and to its echoes. The clutter component **87** can be predicted in large part in the receiver. The edge effects at the conclusion of the repetitive-PN1023 sequence that the PN1023 match filter **80** response exhibits are readily predictable. The PN1023 match filter **80** response to the first 700 symbol epochs of DFS signal succeeding the repetitive-PN1023 sequence is also readily predictable. The PN1023 match filter **80** response to the echoes of the first 700 symbol epochs of DFS signal succeeding the repetitive-PN1023 sequence is not as easily predictable. However, the prediction of clutter component **87** by the receiver is not a matter of much concern in the alternative method for extracting the extended-range cepstrum. This is because the extended-range cepstrum extracted in this alternative method is contaminated principally by the clutter component **86** and very little, if at all, by the clutter component **87**.

The ordinate scale for the clutter components **86** and **87** is expanded in FIGURES 10D, 10E and 10F respective to the principal responses **70''** for sake of illustration. The echo components **71''**, **72''**, **73''** and **74''** are also somewhat larger in amplitude respective to the principal responses **70''** than is the case for a good-quality transmission channel to the receiver. The PN1023 match filter **80** has an auto-correlation function with 60 dB gain against phases of PN1023 sequence other than the initial phase and with 30 dB gain against non-PN1023 signal components.

FIGURE 10E shows the digital subtractor **81** subtrahend signal that the digital delay line **82** supplies in response to the digital subtractor **81** minuend input signal as delayed by one cycle of the repetitive-PN1023 sequence — i.e., by 1023 symbol epochs.

5 FIGURE 10F shows the difference output signal supplied from the digital subtractor **81**. Note that the cepstrum of the initial cycle of PN1023 sequence is separated from the cepstrum of any following PN1023 sequence in the difference output signal supplied from the digital subtractor **81** and usually is not overlapped by components of clutter component **88**. The register **83** temporarily stores this
10 separated cepstrum of the initial cycle of PN1023 sequence from the minuend signal and is connected so its contents are available to the filter-coefficient computer **40**. The filter-coefficient computer **40** can compensate for the readily predictable components of clutter component **87** using *a priori* knowledge extracted from read-only memory. However, only post-echoes delayed more
15 than 150 microseconds or so are likely ever to suffer consequential amounts of contamination by the clutter component **87**. Presuming such processing is performed, the responses to pre-echoes in the extended-range cepstrum temporarily stored in the register **83** are contaminated by leading-edge effects of the PN1023 match filtering, but the portion of this cepstrum containing just
20 responses to post-echoes is not.

The portion of the extended cepstrum stored in the register **83** concerning post-echoes delayed more than 65 microseconds is contaminated with PN1023 match filter **76** response to unknown data as well as to responses to echoes. The portion of the extended cepstrum stored in the register **83** concerning post-
25 echoes delayed more than 65 microseconds is contaminated only with auto-correlation digital filter **80** response to post-echoes of data preceding the repetitive-PN1023 sequence. So, in the great majority of instances, the contamination of echoes delayed more than 65 microseconds is less in the extended cepstrum stored in the register **83** than in the extended cepstrum
30 stored in the register **79**. Accordingly, correlating the separated time-domain response to the post-echoes delayed more than 65 microseconds in the

extended cepstrum stored in the register **83** with the corresponding portion of the cyclically repeating cepstrum pruned per FIGURE 8C is the more reliable basis for the further pruning that cyclically repeating cepstrum. These correlation procedures provide a more reliable basis on which to eliminate repeats of responses to post-echoes and to eliminate aliases of post-echoes delayed more than 95 microseconds that appear as less-delayed post-echoes.

FIGURE 8D depicts the result of eliminations by this alternative method, as well as by the method based on the extended cepstrum stored in the register **79**. With either one of these methods, the FIGURE 8D modifications of the cepstrum are by way of eliminating or reducing temporal components that arose from a cyclic cepstrum based on a PN1023 sequence free from contaminants arising from edge effects, data preceding the repetitive-PN1023 sequence, or DFS signal succeeding the repetitive-PN1023 sequence. Accordingly, such contaminants in the separated time-domain response to post-echoes delayed more than 65 microseconds are not carried forward in appreciable degree into the FIGURE 8D modification of the cyclically repeating cepstrum. The alternative method based on the extended cepstrum stored in the register **83** facilitates the pruning away of repeats of responses to post-echoes and aliases of post-echoes delayed more than 95 microseconds that have smaller energy, since the post-echoes giving rise to these components can be better distinguished from clutter.

The cycles of the cyclically repeating cepstrum become half-cycles of a cepstrum that cyclically repeats in FIGURE 8D without wrap-around, or at least with reduced wrap-around. One cycle of this unwrapped cepstrum provides the improved basis upon which the filter-coefficient computer **40** can calculate filter coefficients for the adaptive channel-equalization and echo-cancellation filtering component FIR filters **33** and **35**.

Receiver designs that dispense with the auto-correlation digital filter **80**, the digital subtractor **81**, the digital delay line **82** and the extended-range cepstrum register **83** are believed to be practical. The separation of pre-echoes from post-echoes is more important to do than pruning away weaker-energy

spurious post-echoes, since weak-energy post-echoes are readily suppressed by data-driven methods of adaptive filtering — e. g., decision-feedback gradient methods. Post-echoes are cancelled by the IIR filter portion of the adaptive channel-equalization and echo-cancellation filtering without appreciably
5 increasing the noise in the filter response. Pre-echo energy is reduced by the FIR filter **33** portion of the adaptive filtering, which in its response replaces the pre-echoes in its input signal with lower-amplitude pre-echoes more advanced in time. This procedure also increases the noise in the adaptive filtering response. Mis-identification of a long-delayed post-echo as a pre-echo undesirably
10 conditions the FIR filter **33** portion of the adaptive filtering to insert spurious pre-echoes in the adaptive filtering response, which insertion procedure also increases the noise in that response.

Receiver designs that average match filter responses from several data fields, better to define static echo conditions, are also contemplated.

15 Especially with the design of receivers capable of handling greater echo ranges extending from the most advanced-in-time pre-echoes to the most delayed-in-time post-echoes, there is a concern that an increased number of multipliers may be needed in the adaptive filtering. Besides the cost in hardware, this tends to exacerbate reduction of C/N by stochastic jitter. Sparse equalization
20 methods have been employed to reduce multiplier requirements and to lessen the reduction of C/N by stochastic jitter. In these methods adaptive bulk delay determines the differential delays between certain kernel taps of the adaptive filters that have non-zero weighting coefficients and accordingly connect to digital multipliers to supply their multiplicand signals. In such receivers the cepstrum
25 provided to the computer **40** from the computer **49** in the FIGURE 5 DTV receiver and from the PN1023 auto-correlation filter **52** in the FIGURE 6 DTV receiver furnishes a basis for allocating the adaptive bulk delays. The computer **40** can be programmed to analyze the cepstrum to select an optimal boundary for the time interval over which the FIR filter **33** time-domain kernel extends for
30 suppressing post echoes.

FIGURE 11 is a diagram of an ATSC digital television signal data frame modified to include two extra data segments at the end of each of its two data fields, which contain the beginning of a repetitive-PN1023 sequence that is used as a training signal for the adaptive filtering that provides channel-equalization and echo-cancellation. The initial, first data segment in each data field differs from that specified by A/53, being modified in that the PN511 sequence is omitted, as well as at least a portion of the triple-PN63 sequence. The repetitive-PN1023 sequence concludes in the portion of that initial data segment thus vacated. The repetitive-PN1023 sequence can be a truncated version of that shown in FIGURES 1A and 1B, being shortened on its concluding end. The ONES in the truncated repetitive-PN1023 sequence will still correspond to +5 carrier modulation values in the digital television signal, and the ZEROS in the truncated repetitive-PN1023 sequence will still correspond to -5 carrier modulation values.

FIGURES 12A, 12B and 12C depict the symbol content of the 313th, 314th and 315th data segments of the even data field of a previous data frame in a FIGURE 11 DTV signal broadcast in accordance with the invention. FIGURES 12D and 12E graph the symbol content of the initial and second data segments of the succeeding odd data field in the current data frame. FIGURES 12F, 12G and 12H depict the symbol content of the 313th, 314th and 315th data segments of that succeeding odd data field. FIGURES 12I and 12J graph the symbol content of the initial and second data segments data segment of the even data field of the next data frame.

The second through 313th data segments of the data fields can be the same as those specified in A/53. The third through 312th data segments of the odd field of the current frame, which would occur in the time interval between the conclusion of the second data segment shown in FIGURE 12E and the beginning of the 313th data segment shown in FIGURE 12F are omitted from the drawing for reasons of economy of drawing.

The 314th and 315th data segments concluding each data field contain the first 1664 symbols of the 2368 repetitive-PN1023-sequence ECR signal, which continues into the initial data segments of the succeeding data fields. FIGURES 12B and 12C show the first 1664 symbols of the repetitive-PN1023-sequence ECR signal inserted into the 314th and 315th data segments of the even data field of the data frame previous to the current data frame depicted in FIGURES 12D, 12E, 12F, 12G and 12H. FIGURES 12G and 12H show the first 1664 symbols of the repetitive-PN1023-sequence ECR signal inserted into the 314th and 315th data segments of the odd data field of the current data frame. The data segment synchronizing (DSS) signals of the 314th and 315th data segments of each data field are incorporated within the repetitive-PN1023-sequence ECR signal transmitted during those data segments. So is the DSS signal at the beginning of the initial data segment of the succeeding field, as depicted in FIGURES 12D and 12I.

The repetitive-PN1023 sequence of FIGURES 12B, 12C and 12D varies between -5 and +5 modulation levels in the 8-VSB signal, as A/53 specifies such modulation levels. The repetitive-PN1023 sequence of FIGURES 12G, 12H and 12I also varies between -5 and +5 modulation levels. These modulation levels for the repetitive-PN1023 sequences facilitate the 4-symbol DSS sequences being incorporated within these repetitive-PN1023 sequences.

The initial data segment of an odd data field, as shown in FIGURE 12D, and the initial data segment of a succeeding even data field, as shown in FIGURE 12I, each begin with a 4-symbol data segment sync (DSS) sequence incorporated within a portion of one of the 2368-symbol repetitive-PN1023 sequences followed by the concluding 700 symbols of that sequence. The conclusion of the repetitive-PN1023 sequence is followed by a 24-symbol mode code, and a 104-symbol reserved portion that concludes the data segment.

Because there are only 315 data segments per data field for the signal of FIGURES 12A, 12B, 12C, 12D, 12E, 12F, 12G, 12H, 12I and 12J, rather than 316 data segments per data field, a transmitter for this signal will differ somewhat

from the FIGURE 4 transmitter. Besides a change in the general clocking, the transmitter for this 315-data-segments-per-field signal, will not include the ROM **13** for storing PN511 and triple-PN63 sequences. The timing of the DFS assembler **12**, the multiplexer **11** for inserting the DFS signal, and the multiplexer **17** for inserting training signal will be affected in ways obvious to one of ordinary skill in the art of digital communications system design. The addressing of the ROM **18** for generating repetitive-PN1023 training signal will also be affected in a way obvious to one of ordinary skill in the art of digital communications system design.

10 A receiver for the signal of FIGURES 12A, 12B, 12C, 12D, 12E, 12F, 12G, 12H, 12I and 12J with 315 data segments per data field will differ somewhat from the receiver for the signal of FIGURES 3A, 3B, 3C, 3D, 3E, 3F, 3G, 3H, 3I, 3J, 3K and 3L with 316 data segments per data field. The FIGURE 5 receiver portion is modified in regard to timing the gate **43** to select one cycle of
15 repetitive-PN1023 sequence from each training signal to be used by the computer **44** for computing the DFT power spectrum. The FIGURE 6 receiver portion is modified in regard to timing the multiplexer **50** to select one cycle of repetitive-PN1023 sequence from each training signal for application to the shift register **51** to be recycled throughout the following data field. Minor modifications
20 in the application of the cepstrum to the filter-coefficient computer **52** will need to be made in both the FIGURE 5 and FIGURE 6 receiver portions.

 The FIGURE 7 receiver portion will be modified with respect to the synchronizing signal extraction circuitry **57** and with respect to the receiver clocking and timing circuitry **58**. The portions of the synchronizing signal
25 extraction circuitry **57** having to do with the extraction of the DSS signals will remain pretty much the same, but the portions having to do with the extraction of the DFS signals must be changed because the PN511 sequence and the triple-PN63 sequence of the A/53 standard are no longer available. The data-field-synchronizing signal can be generated in response to the occurrence in the
30 baseband DTV signal of a cycle of PN1023 sequence of specific phase a prescribed time later than the occurrence of a DSS sequence, for example. The

receiver clocking and timing circuitry **58** will be modified to include a counter that counts data segments with the data segment count being reset every 315 data segments by the data-field-synchronizing signal generated by the modified synchronizing signal extraction circuitry **57**.

5 A variant of the 316-data-segment-per-field signal of FIGURES 3A, 3B, 3C, 3D, 3E, 3F, 3G, 3H, 3I, 3J, 3K and 3L begins the repetitive-PN1023-sequence training signal 28 symbol epochs later in the 314th data segment of each data field, to permit transmission of 24 symbols that will terminate the trellis coding lattice with a set of standard states in the trellis decoder before trellis coding is
10 discontinued as the training signal begins. Trellis coding then starts afresh from this set of standard states in the second data segment of each data field, and no twelve-symbol precode is included at the end of the first data segment. If this variant is transmitted, the FIGURE 4 transmitter is modified to omit the temporary storage **10** for the last twelve symbols of the 313th data segment of the preceding
15 data field, and the DFS signal assembler **12** is modified. Provision will also be made to terminate the trellis coding lattice just before the 101st symbol of the 314th data segment of each data field. A read-only memory addressed by the lattice states stored at the conclusion of the 313th data segment in a trellis decoder located at the transmitter can be used for terminating the trellis coding
20 lattice, for example. The changes in clocking the trellis decoder are obvious to one of ordinary skill in the art of digital communications system design.

 A variant of the 315-data-segment-per-field signal of FIGURES 12A, 12B, 12C, 12D, 12E, 12F, 12G, 12H, 12I and 12J that begins the repetitive-PN1023-sequence training signal 28 symbol epochs later in the 314th data segment of
25 each data field, to permit transmission of symbols that will terminate the trellis coding lattice with a set of standard states in the trellis decoder before trellis coding is discontinued as the training signal begins, is also possible.

 In still other training signals embodying aspects of the invention, the beginning of the repetitive-PN1023 sequence may be deferred for several symbol

epochs to accommodate the inclusion of a prescribed annunciator sequence to announce the subsequent arrival of the repetitive-PN1023 sequence.

Industrial Applicability

- 5 The training signals described in the foregoing application facilitate adaptive equalization in DTV receivers to compensate for imperfections in DTV signals received via cable transmission and via satellite transmission, as well as DTV signals received via terrestrial over-the-air broadcasting.

What is claimed is:

1. A method of structuring each of a succession of consecutive data fields for digital television broadcasting to at least one receiver having adaptive equalization and echo suppression filtering therein, said method comprising
5 steps of:
 - dividing each said data field into a prescribed number of successive data segments of equal durations, each containing a prescribed number of plural-modulation-level symbols; and
 - beginning each data segment with a respective data segment
10 synchronizing sequence of common type, which data segment synchronizing sequence consists of symbols of first and second modulation levels as used in said plural-modulation-level symbols; said method being improved to further comprise a step of:
 - including within consecutive data segments in a first portion of each said
15 data field a prescribed number more than one of consecutive cycles of a particular pseudo-random noise sequence consisting of symbols of said first and said second modulation levels, a full cycle of said particular pseudo-random noise sequence having a duration longer than the duration of each said data segment, and said consecutive cycles of said particular pseudo-random noise
20 sequence incorporating at least one said data segment synchronizing sequence of said common type.
2. The method of claim 1, wherein said prescribed number more than one of consecutive cycles of a particular pseudo-random noise sequence is at least two.
3. The method of claim 1, wherein said particular pseudo-random noise
25 sequence is a PN1023 sequence.

4. A transmitter for digital television signals broadcast in accordance with the method of claim 3.
5. A receiver for digital television signals broadcast in accordance with the method of claim 3, said receiver comprising:
- 5 front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for reception;
- demodulator and analog-to-digital conversion circuitry for recovering a digitized baseband broadcast digital television signal from said amplified
- 10 intermediate-frequency signal, said demodulator and analog-to-digital conversion circuitry connected for receiving said amplified intermediate-frequency signal from said front-end circuitry;
- gating circuitry for selecting from each occurrence of said training signal in the digitized baseband broadcast digital television signal recovered by said
- 15 demodulator and analog-to-digital conversion circuitry a respective set of successive digital samples of 1023 symbol epochs duration;
- DFT computer apparatus for computing the discrete Fourier transform of the power spectrum of said respective set of successive digital samples of 1023 symbol epochs duration;
- 20 circuitry for generating a discrete Fourier transform characterizing the actual transmission channel by determining the quotient of
- each term of said discrete Fourier transform of the power spectrum of said respective set of successive digital samples of 1023 symbol epochs duration that said DFT computer apparatus computes, and

the corresponding term of a discrete Fourier transform indicative of the response of an ideal transmission channel to said training signal;

inverse-discrete-Fourier-transform circuitry for computing the inverse-Fourier transform of said discrete Fourier transform characterizing said actual
5 transmission channel; and

adaptive channel-equalization and echo-cancellation filtering connected for responding to said digitized baseband broadcast digital television signal with a response that is adapted by adjustment of the weighting coefficients of said adaptive channel-equalization and echo-cancellation filtering in response to said
10 inverse-Fourier transform.

6. A receiver for digital television signals broadcast in accordance with the method of claim 3, said receiver comprising:

front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for
15 reception;

demodulator and analog-to-digital conversion circuitry for recovering a digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion circuitry connected for receiving said amplified intermediate-frequency signal
20 from said front-end circuitry;

match filtering apparatus of cyclical type, connected for selecting from each occurrence of said training signal in said digitized baseband broadcast digital television signal from said demodulator and analog-to-digital conversion circuitry a respective set of successive digital samples of 1023 symbol epochs
25 duration, said match filtering apparatus performing cyclic PN1023 autocorrelation filtering on each said respective set of successive digital samples of 1023 symbol

epochs duration to generate a cepstrum characterizing the transmission channel to said receiver for digital television signals; and

adaptive channel-equalization and echo-cancellation filtering connected for responding to said digitized baseband broadcast digital television signal with
5 a response that is adapted by adjustment of the weighting coefficients of said adaptive channel-equalization and echo-cancellation filtering in response to said cepstrum.

7. A receiver for digital television signals broadcast in accordance with the
10 method of claim 3, said receiver comprising:

front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for reception;

demodulator and analog-to-digital conversion circuitry for recovering a
15 digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion circuitry connected for receiving said amplified intermediate-frequency signal from said front-end circuitry;

a direct-component-suppression filter connected to receive as its input
20 signal said digitized baseband broadcast digital television signal from said demodulator and analog-to-digital conversion circuitry, said direct-component-suppression filter connected to supply a response to said digitized baseband broadcast digital television signal that suppresses any direct component attributable to detection of a pilot carrier accompanying said radio-frequency
25 broadcast digital television signal selected for reception;

match filtering apparatus of non-cyclical type, connected for performing PN1023 autocorrelation filtering on the response of said direct-component-suppression filter, to supply a match filter response;

5 a comb filter connected to receive as its input signal said match filter response and to supply a comb filter response which differentially combines said match filter response with itself as delayed 1023 symbol epochs, said comb filter response including an extended cepstrum characterizing the transmission channel to said receiver for digital television signals, which extended cepstrum is generated responsive to the consecutive cycles of said PN1023 sequence in
10 each data field;

an extended-cepstrum register connected for selecting from said comb filter response the cepstrum generated responsive to the consecutive cycles of said PN1023 sequence in each data field, to be temporarily stored in said extended-cepstrum register; and

15 adaptive channel-equalization and echo-cancellation filtering connected for responding to said digitized baseband broadcast digital television signal with a response that is adapted by adjustment of the weighting coefficients of said adaptive channel-equalization and echo-cancellation filtering in response to said extended cepstrum.

20

8. A receiver for digital television signals broadcast in accordance with the method of claim 3, said receiver comprising:

front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for
25 reception;

demodulator and analog-to-digital conversion circuitry for recovering a digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion circuitry connected for receiving said amplified intermediate-frequency signal
5 from said front-end circuitry;

gating circuitry for selecting from each occurrence of said training signal in the digitized baseband broadcast digital television signal recovered by said demodulator and analog-to-digital conversion circuitry a respective set of successive digital samples of 1023 symbol epochs duration;

10 DFT computer apparatus for computing the discrete Fourier transform of the power spectrum of said respective set of successive digital samples of 1023 symbol epochs duration;

circuitry for generating a discrete Fourier transform characterizing the actual transmission channel by determining the quotient of

15 each term of said discrete Fourier transform of the power spectrum of said respective set of successive digital samples of 1023 symbol epochs duration that said DFT computer apparatus computes, and

the corresponding term of a discrete Fourier transform indicative of the response of an ideal transmission channel to said training signal;

20 inverse-discrete-Fourier-transform circuitry for computing the inverse-Fourier transform of said discrete Fourier transform characterizing said actual transmission channel;

a direct-component-suppression filter connected to receive as its input signal said digitized baseband broadcast digital television signal from said
25 demodulator and analog-to-digital conversion circuitry, said direct-component-

suppression filter connected to supply a response to said digitized baseband broadcast digital television signal that suppresses any direct component attributable to detection of a pilot carrier accompanying said radio-frequency broadcast digital television signal selected for reception;

- 5 match filtering apparatus of non-cyclical type, connected for performing PN1023 autocorrelation filtering on the response of said direct-component-suppression filter, to supply a match filter response;

10 a comb filter connected to receive as its input signal said match filter response and to supply a comb filter response which differentially combines said match filter response with itself as delayed 1023 symbol epochs, said comb filter response including extended cepstrums characterizing the transmission channel to said receiver for digital television signals, one of said extended cepstrums being generated responsive to the consecutive cycles of said PN1023 sequence in each data field;

- 15 an extended-cepstrum register connected for selecting from said comb filter response the extended cepstrum generated responsive to the consecutive cycles of said PN1023 sequence in each data field, to be temporarily stored in said extended-cepstrum register;

20 a computer in which a cyclic repetition of the inverse-Fourier transform of said discrete Fourier transform characterizing said actual transmission channel is generated and is pruned in accordance with the extended cepstrum temporarily stored in said extended-cepstrum register to generate a channel impulse response without wrap-around; and

- 25 adaptive channel-equalization and echo-cancellation filtering connected for responding to said digitized baseband broadcast digital television signal with a response that is adapted by adjustment of the weighting coefficients of said

adaptive channel-equalization and echo-cancellation filtering in response to said channel impulse response without wrap-around.

9. A receiver for digital television signals broadcast in accordance with the
5 method of claim 3, said receiver comprising:

front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for reception;

- 10 demodulator and analog-to-digital conversion circuitry for recovering a digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion circuitry connected for receiving said amplified intermediate-frequency signal from said front-end circuitry;

- 15 match filtering apparatus of cyclical type, connected for selecting from each occurrence of said training signal in said digitized baseband broadcast digital television signal from said demodulator and analog-to-digital conversion circuitry a respective set of successive digital samples of 1023 symbol epochs duration, said match filtering apparatus performing cyclic PN1023 autocorrelation filtering on each said respective set of successive digital samples of 1023 symbol
20 epochs duration to generate a cepstrum characterizing the transmission channel to said receiver for digital television signals;

- a direct-component-suppression filter connected to receive as its input signal said digitized baseband broadcast digital television signal from said demodulator and analog-to-digital conversion circuitry, said direct-component-
25 suppression filter connected to supply a response to said digitized baseband broadcast digital television signal that suppresses any direct component

attributable to detection of a pilot carrier accompanying said radio-frequency broadcast digital television signal selected for reception;

match filtering apparatus of non-cyclical type, connected for performing PN1023 autocorrelation filtering on the response of said direct-component-suppression filter, to supply a match filter response;

a comb filter connected to receive as its input signal said match filter response and to supply a comb filter response which differentially combines said match filter response with itself as delayed 1023 symbol epochs, said comb filter response including extended cepstrums characterizing the transmission channel to said receiver for digital television signals, one of said extended cepstrums being generated responsive to the consecutive cycles of said PN1023 sequence in each data field;

an extended-cepstrum register connected for selecting from said comb filter response the extended cepstrum generated responsive to the consecutive cycles of said PN1023 sequence in each data field, to be temporarily stored in said extended-cepstrum register;

a computer in which a cyclic repetition is generated of the cepstrum generated by said match filtering apparatus of cyclical type and is pruned in accordance with the extended cepstrum temporarily stored in said extended-cepstrum register to generate a channel impulse response without wrap-around; and

adaptive channel-equalization and echo-cancellation filtering connected for responding to said digitized baseband broadcast digital television signal with a response that is adapted by adjustment of the weighting coefficients of said adaptive channel-equalization and echo-cancellation filtering in response to said channel impulse response without wrap-around.

10. The method of claim 1, wherein said particular pseudo-random noise sequence is a PN1023 sequence, further comprising steps of:

forward-error-correction coding data to generate forward-error-correction
5 coded data;

convolutionally interleaving said forward-error-correction coded data to generate convolutionally interleaved forward-error-correction coded data; and

processing said convolutionally interleaved forward-error-correction coded data for inclusion in consecutive data segments within a prescribed second
10 portion of each said data field.

11. A transmitter for digital television signals broadcast in accordance with the method of claim 10.

15 12. A receiver for digital television signals broadcast in accordance with the method of claim 10, said receiver comprising:

front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for reception;

20 demodulator and analog-to-digital conversion circuitry for recovering a digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion

circuitry connected for receiving said amplified intermediate-frequency signal from said front-end circuitry;

gating circuitry for selecting from each occurrence of said training signal in the digitized baseband broadcast digital television signal recovered by said demodulator and analog-to-digital conversion circuitry a respective set of
5 successive digital samples of 1023 symbol epochs duration;

DFT computer apparatus for computing the discrete Fourier transform of the power spectrum of said respective set of successive digital samples of 1023 symbol epochs duration;

10 circuitry for generating a discrete Fourier transform characterizing the actual transmission channel by determining the quotient of

each term of said discrete Fourier transform of the power spectrum of said respective set of successive digital samples of 1023 symbol epochs duration that said DFT computer apparatus computes, and

15 the corresponding term of a discrete Fourier transform indicative of the response of an ideal transmission channel to said training signal;

inverse-discrete-Fourier-transform circuitry for computing the inverse-Fourier transform of said discrete Fourier transform characterizing said actual transmission channel;

20 adaptive channel-equalization and echo-cancellation filtering connected for responding to said digitized baseband broadcast digital television signal with a response that is adapted by adjustment of the weighting coefficients of said adaptive channel-equalization and echo-cancellation filtering in response to said inverse-Fourier transform;

a symbol decoder for decoding the response of said adaptive channel-equalization and echo-cancellation filtering to recover interleaved data;

a convolutional de-interleaver connected for de-interleaving the interleaved data recovered by said symbol decoder to generate packets of de-interleaved data;

error-detection-and-correction circuitry connected for detecting any errors in each of said packets of de-interleaved data, said error-detection-and-correction circuitry connected for supplying said packets of de-interleaved data with each one of said packets that had fewer than a prescribed number of errors having been corrected;

a data de-randomizer connected for receiving from said error-detection-and-correction circuitry said packets of de-interleaved data with each one of said packets that had fewer than a prescribed number of errors having been corrected, and for generating a data de-randomizer output signal by exclusive-ORing said de-interleaved data with a prescribed de-randomizing signal; and

a packet sorter connected for supplying in each of a plurality of output signals therefrom a particular set of identifiable data packets sorted from said data de-randomizer output signal in response to a packet identification signal for each data packet therein not left in error by said error-detection-and-correction circuitry.

13. A receiver for digital television signals broadcast in accordance with the method of claim 10, said receiver comprising:

front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for reception;

5 demodulator and analog-to-digital conversion circuitry for recovering a digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion circuitry connected for receiving said amplified intermediate-frequency signal from said front-end circuitry;

10 front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for reception;

15 demodulator and analog-to-digital conversion circuitry for recovering a digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion circuitry connected for receiving said amplified intermediate-frequency signal from said front-end circuitry;

20 match filtering apparatus of cyclical type, connected for selecting from each occurrence of said training signal in said digitized baseband broadcast digital television signal from said demodulator and analog-to-digital conversion circuitry a respective set of successive digital samples of 1023 symbol epochs duration, said match filtering apparatus performing cyclic PN1023 autocorrelation filtering on each said respective set of successive digital samples of 1023 symbol epochs duration to generate a cepstrum characterizing the transmission channel to said receiver for digital television signals;

25 adaptive channel-equalization and echo-cancellation filtering connected for responding to said digitized baseband broadcast digital television signal with

a response that is adapted by adjustment of the weighting coefficients of said adaptive channel-equalization and echo-cancellation filtering in response to said cepstrum;

5 a symbol decoder for decoding the response of said adaptive channel-equalization and echo-cancellation filtering to recover interleaved data;

a convolutional de-interleaver connected for de-interleaving the interleaved data recovered by said symbol decoder to generate packets of de-interleaved data;

10 error-detection-and-correction circuitry connected for detecting any errors in each of said packets of de-interleaved data, said error-detection-and-correction circuitry connected for supplying said packets of de-interleaved data with each one of said packets that had fewer than a prescribed number of errors having been corrected;

15 a data de-randomizer connected for receiving from said error-detection-and-correction circuitry said packets of de-interleaved data with each one of said packets that had fewer than a prescribed number of errors having been corrected, and for generating a data de-randomizer output signal by exclusive-ORing said de-interleaved data with a prescribed de-randomizing signal; and

20 a packet sorter connected for supplying in each of a plurality of output signals therefrom a particular set of identifiable data packets sorted from said data de-randomizer output signal in response to a packet identification signal for each data packet therein not left in error by said error-detection-and-correction circuitry.

25

14. A receiver for digital television signals broadcast in accordance with the method of claim 10, said receiver comprising:

front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for reception;

demodulator and analog-to-digital conversion circuitry for recovering a digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion circuitry connected for receiving said amplified intermediate-frequency signal from said front-end circuitry;

a direct-component-suppression filter connected to receive as its input signal said digitized baseband broadcast digital television signal from said demodulator and analog-to-digital conversion circuitry, said direct-component-suppression filter connected to supply a response to said digitized baseband broadcast digital television signal that suppresses any direct component attributable to detection of a pilot carrier accompanying said radio-frequency broadcast digital television signal selected for reception;

match filtering apparatus of non-cyclical type, connected for performing PN1023 autocorrelation filtering on the response of said direct-component-suppression filter, to supply a match filter response;

a comb filter connected to receive as its input signal said match filter response and to supply a comb filter response which differentially combines said match filter response with itself as delayed 1023 symbol epochs, said comb filter response including an extended cepstrum characterizing the transmission channel to said receiver for digital television signals, which extended cepstrum is

generated responsive to the consecutive cycles of said PN1023 sequence in each data field;

an extended-cepstrum register connected for selecting from said comb filter response the cepstrum generated responsive to the consecutive cycles of said PN1023 sequence in each data field, to be temporarily stored in said
5 extended-cepstrum register;

adaptive channel-equalization and echo-cancellation filtering connected for responding to said digitized baseband broadcast digital television signal with a response that is adapted by adjustment of the weighting coefficients of said
10 adaptive channel-equalization and echo-cancellation filtering in response to said extended cepstrum;

a symbol decoder for decoding the response of said adaptive channel-equalization and echo-cancellation filtering to recover interleaved data;

a convolutional de-interleaver connected for de-interleaving the
15 interleaved data recovered by said symbol decoder to generate packets of de-interleaved data;

error-detection-and-correction circuitry connected for detecting any errors in each of said packets of de-interleaved data, said error-detection-and-correction circuitry connected for supplying said packets of de-interleaved data
20 with each one of said packets that had fewer than a prescribed number of errors having been corrected;

a data de-randomizer connected for receiving from said error-detection-and-correction circuitry said packets of de-interleaved data with each one of said packets that had fewer than a prescribed number of errors having been corrected,
25 and for generating a data de-randomizer output signal by exclusive-ORing said de-interleaved data with a prescribed de-randomizing signal; and

a packet sorter connected for supplying in each of a plurality of output signals therefrom a particular set of identifiable data packets sorted from said data de-randomizer output signal in response to a packet identification signal for each data packet therein not left in error by said error-detection-and-correction
5 circuitry.

15. The method of claim 10 wherein said step of processing said convolutionally interleaved forward-error-correction coded data for inclusion in data segments within a prescribed first portion of each said data field includes
10 sub-steps of:

trellis coding said convolutionally interleaved forward-error-correction coded data to generate trellis-coded data; and

apportioning said trellis-coded data among data segments within said prescribed second portion of each said data field.

15

16. A transmitter for digital television signals broadcast in accordance with the method of claim 15.

17. A receiver for digital television signals broadcast in accordance with the
20 method of claim 15, said receiver comprising:

front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for reception;

demodulator and analog-to-digital conversion circuitry for recovering a digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion circuitry connected for receiving said amplified intermediate-frequency signal
5 from said front-end circuitry;

gating circuitry for selecting from each occurrence of said training signal in the digitized baseband broadcast digital television signal recovered by said demodulator and analog-to-digital conversion circuitry a respective set of successive digital samples of 1023 symbol epochs duration;

10 DFT computer apparatus for computing the discrete Fourier transform of the power spectrum of said respective set of successive digital samples of 1023 symbol epochs duration;

circuitry for generating a discrete Fourier transform characterizing the actual transmission channel by determining the quotient of

15 each term of said discrete Fourier transform of the power spectrum of said respective set of successive digital samples of 1023 symbol epochs duration that said DFT computer apparatus computes, and

the corresponding term of a discrete Fourier transform indicative of the response of an ideal transmission channel to said training signal;

20 inverse-discrete-Fourier-transform circuitry for computing the inverse-Fourier transform of said discrete Fourier transform characterizing said actual transmission channel;

adaptive channel-equalization and echo-cancellation filtering connected for responding to said digitized baseband broadcast digital television signal with
25 a response that is adapted by adjustment of the weighting coefficients of said

adaptive channel-equalization and echo-cancellation filtering in response to said inverse-Fourier transform;

a trellis decoder for decoding the response of said adaptive channel-equalization and echo-cancellation filtering to recover interleaved data;

- 5 a convolutional de-interleaver connected for de-interleaving the interleaved data recovered by said symbol decoder to generate packets of de-interleaved data;

- error-detection-and-correction circuitry connected for detecting any errors in each of said packets of de-interleaved data, said error-detection-and-
10 correction circuitry connected for supplying said packets of de-interleaved data with each one of said packets that had fewer than a prescribed number of errors having been corrected;

- a data de-randomizer connected for receiving from said error-detection-and-correction circuitry said packets of de-interleaved data with
15 each one of said packets that had fewer than a prescribed number of errors having been corrected, and for generating a data de-randomizer output signal by exclusive-ORing said de-interleaved data with a prescribed de-randomizing signal; and

- a packet sorter connected for supplying in each of a plurality of output
20 signals therefrom a particular set of identifiable data packets sorted from said data de-randomizer output signal in response to a packet identification signal for each data packet therein not left in error by said error-detection-and-correction circuitry.

18. A receiver for digital television signals broadcast in accordance with the method of claim 15, said receiver comprising:

front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for
5 reception;

demodulator and analog-to-digital conversion circuitry for recovering a digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion circuitry connected for receiving said amplified intermediate-frequency signal
10 from said front-end circuitry;

front-end circuitry for supplying an amplified intermediate-frequency signal responsive to a radio-frequency broadcast digital television signal selected for reception;

demodulator and analog-to-digital conversion circuitry for recovering a
15 digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion circuitry connected for receiving said amplified intermediate-frequency signal from said front-end circuitry;

match filtering apparatus of cyclical type, connected for selecting from
20 each occurrence of said training signal in said digitized baseband broadcast digital television signal from said demodulator and analog-to-digital conversion circuitry a respective set of successive digital samples of 1023 symbol epochs duration, said match filtering apparatus performing cyclic PN1023 autocorrelation filtering on each said respective set of successive digital samples of 1023 symbol
25 epochs duration to generate a cepstrum characterizing the transmission channel to said receiver for digital television signals;

adaptive channel-equalization and echo-cancellation filtering connected for responding to said digitized baseband broadcast digital television signal with a response that is adapted by adjustment of the weighting coefficients of said adaptive channel-equalization and echo-cancellation filtering in response to said cepstrum;

a trellis decoder for decoding the response of said adaptive channel-equalization and echo-cancellation filtering to recover interleaved data;

a convolutional de-interleaver connected for de-interleaving the interleaved data recovered by said symbol decoder to generate packets of de-interleaved data;

error-detection-and-correction circuitry connected for detecting any errors in each of said packets of de-interleaved data, said error-detection-and-correction circuitry connected for supplying said packets of de-interleaved data with each one of said packets that had fewer than a prescribed number of errors having been corrected;

a data de-randomizer connected for receiving from said error-detection-and-correction circuitry said packets of de-interleaved data with each one of said packets that had fewer than a prescribed number of errors having been corrected, and for generating a data de-randomizer output signal by exclusive-ORing said de-interleaved data with a prescribed de-randomizing signal; and

a packet sorter connected for supplying in each of a plurality of output signals therefrom a particular set of identifiable data packets sorted from said data de-randomizer output signal in response to a packet identification signal for each data packet therein not left in error by said error-detection-and-correction circuitry.

19. A receiver for digital television signals broadcast in accordance with the method of claim 15, said receiver comprising:

front-end circuitry for supplying an amplified intermediate-frequency signal
5 responsive to a radio-frequency broadcast digital television signal selected for reception;

demodulator and analog-to-digital conversion circuitry for recovering a digitized baseband broadcast digital television signal from said amplified intermediate-frequency signal, said demodulator and analog-to-digital conversion
10 circuitry connected for receiving said amplified intermediate-frequency signal from said front-end circuitry;

a direct-component-suppression filter connected to receive as its input signal said digitized baseband broadcast digital television signal from said demodulator and analog-to-digital conversion circuitry, said direct-component-
15 suppression filter connected to supply a response to said digitized baseband broadcast digital television signal that suppresses any direct component attributable to detection of a pilot carrier accompanying said radio-frequency broadcast digital television signal selected for reception;

match filtering apparatus of non-cyclical type, connected for performing
20 PN1023 autocorrelation filtering on the response of said direct-component-suppression filter, to supply a match filter response;

a comb filter connected to receive as its input signal said match filter response and to supply a comb filter response which differentially combines said match filter response with itself as delayed 1023 symbol epochs, said comb filter
25 response including an extended cepstrum characterizing the transmission channel to said receiver for digital television signals, which extended cepstrum is

generated responsive to the consecutive cycles of said PN1023 sequence in each data field;

an extended-cepstrum register connected for selecting from said comb filter response the cepstrum generated responsive to the consecutive cycles of said PN1023 sequence in each data field, to be temporarily stored in said
5 extended-cepstrum register;

adaptive channel-equalization and echo-cancellation filtering connected for responding to said digitized baseband broadcast digital television signal with a response that is adapted by adjustment of the weighting coefficients of said
10 adaptive channel-equalization and echo-cancellation filtering in response to said extended cepstrum;

a trellis decoder for decoding the response of said adaptive channel-equalization and echo-cancellation filtering to recover interleaved data;

a convolutional de-interleaver connected for de-interleaving the
15 interleaved data recovered by said symbol decoder to generate packets of de-interleaved data;

error-detection-and-correction circuitry connected for detecting any errors in each of said packets of de-interleaved data, said error-detection-and-correction circuitry connected for supplying said packets of de-interleaved data
20 with each one of said packets that had fewer than a prescribed number of errors having been corrected;

a data de-randomizer connected for receiving from said error-detection-and-correction circuitry said packets of de-interleaved data with each one of said packets that had fewer than a prescribed number of errors having been corrected,
25 and for generating a data de-randomizer output signal by exclusive-ORing said de-interleaved data with a prescribed de-randomizing signal; and

- a packet sorter connected for supplying in each of a plurality of output signals therefrom a particular set of identifiable data packets sorted from said data de-randomizer output signal in response to a packet identification signal for each data packet therein not left in error by said error-detection-and-correction
- 5 circuitry.

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FIG. 1A

100111000110100011111111101111110100111101
11010101000110101111111100011111001110110001
00101011010001001111110101011101101000010111
11010000110111101111001010010000011001100111
00110010000110001101110111110001001100110101
10011110010010100001000111010111100110001000
11011011111101100111010100100110110010111010
00000011110000110100101111110000011100100110
00001011010010001111001111010001010111110010
00110000111110101101101100110110100111011110
10010010111001000000000110000001110100011001
11111100101111000000010010000101001101001101
11110111001101000001111110011011100011100001
11000101100011000101111011000010101010100101
01011000101001011001100001001101010101111010
10001011011110001100100111100010101001100101
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00010001000101110111000001000010010110101000
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11011100101100000000101000001001110010101000
00010111000100000011011000111101011101011000
01100101011100001000001010110010010010001001
00111010010100111000110100011111111110111111
10100111101110101010001101011111111000111110
01110110001001010110100010011111101010111011
01000010111110100001101111011110010100100000
11001100111001100100001100011011101111100010
01100110101100111100100101000010001110101111

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FIG. 1B

0011000100011011011111011001110101001001101
10010111010000000111100001101001011111100000
11100100110000010110100100011110011110100010
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00111011110100100101110010000000001100000011
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01111100010011001101011001111001001010000100
01110101111001100010001101101111110110011101
01001001101100101110100000001111000011010010
11111100000111001001100000101101001000111100
11110100010101111100100011000011111010110110
1100110110100111011110100100101110010000000

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FIG. 2

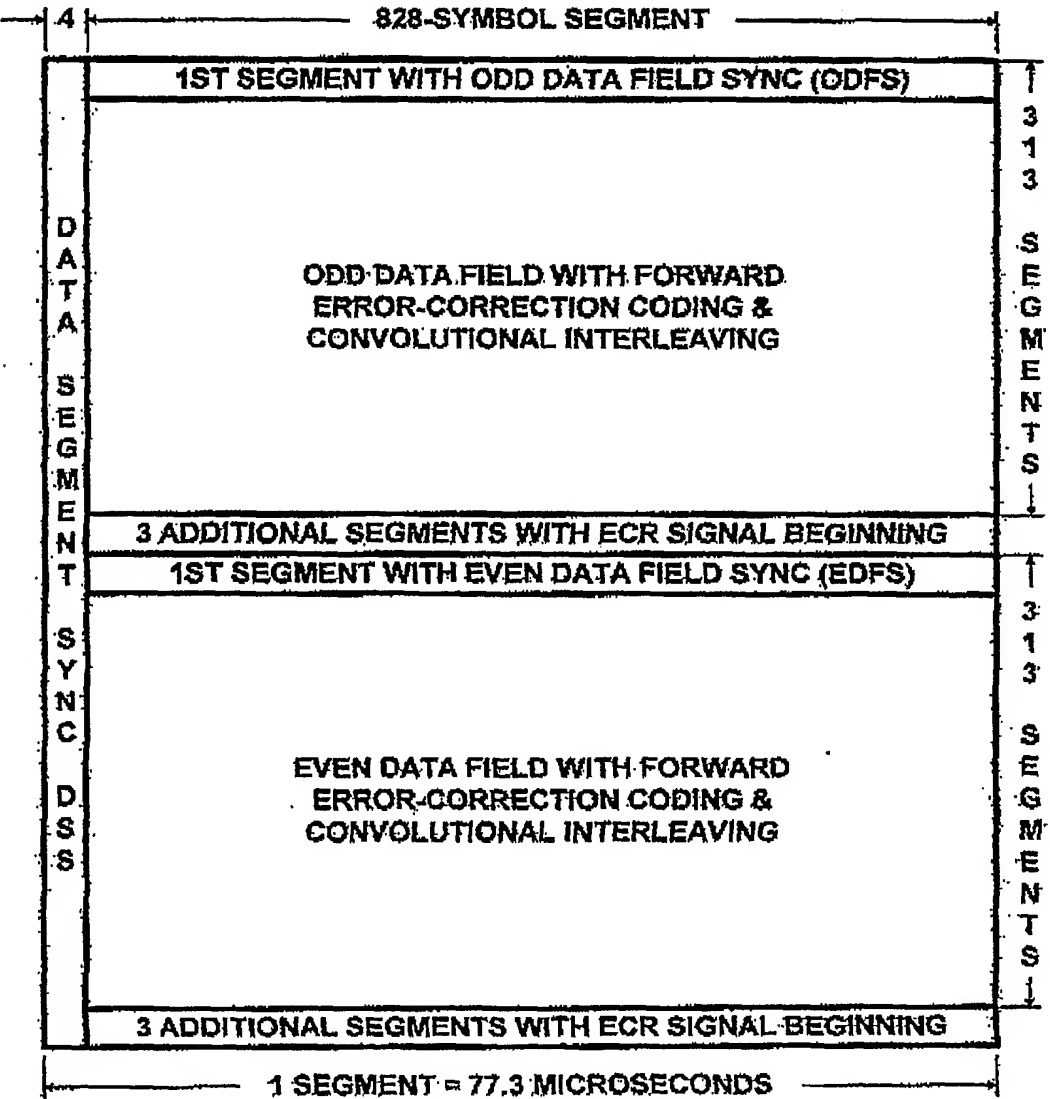


FIG. 3A

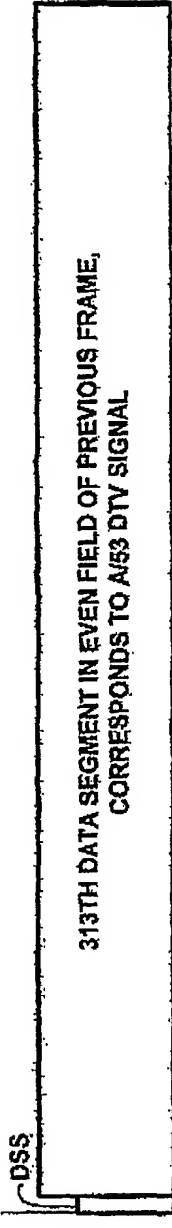


FIG. 3B

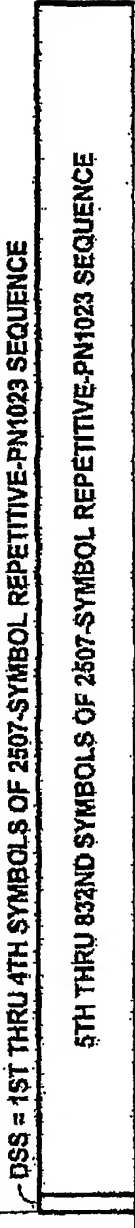


FIG. 3C

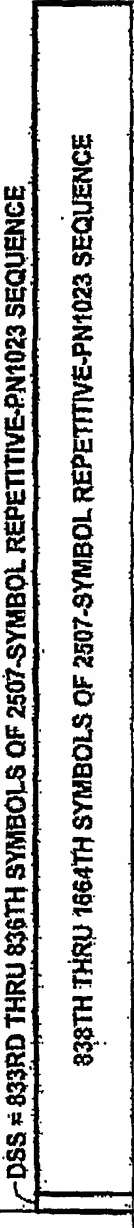


FIG. 3D

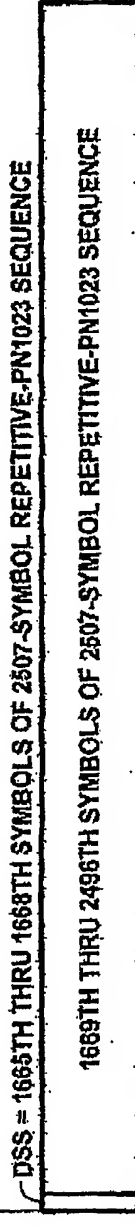


FIG. 3E

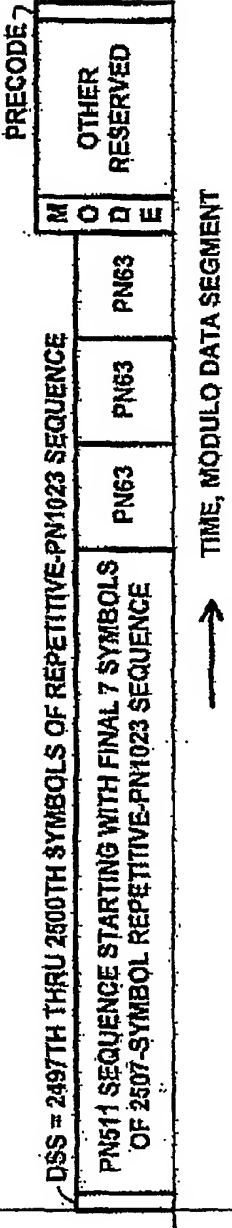
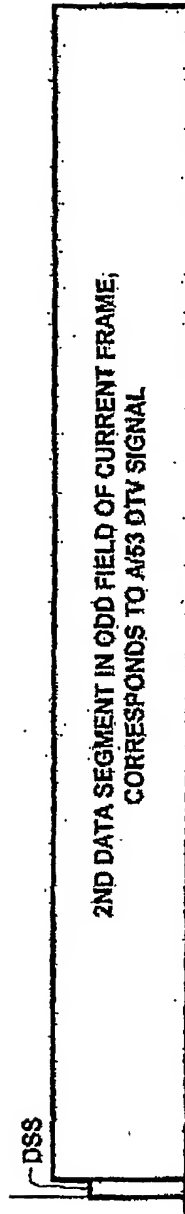


FIG. 3F



3RD THRU 309TH DATA SEGMENTS OF ODD FIELD OF CURRENT FRAME
(HERE OMITTED) CORRESPOND TO THOSE IN A/53 DTV SIGNAL

FIG. 3G

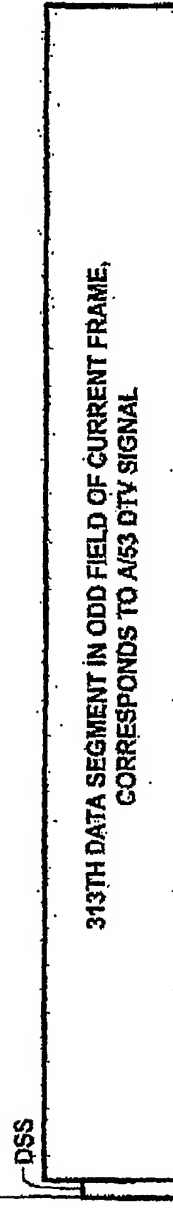
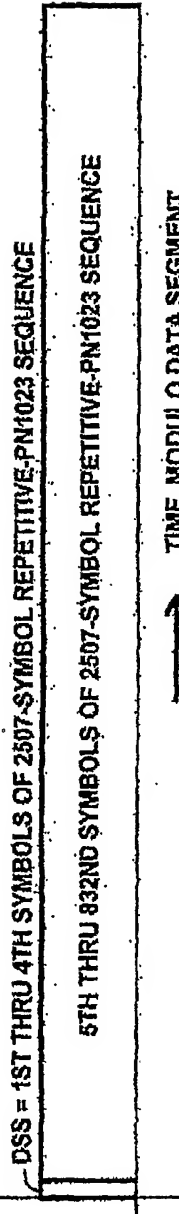


FIG. 3H



→ TIME, MODULO DATA SEGMENT

FIG. 3I

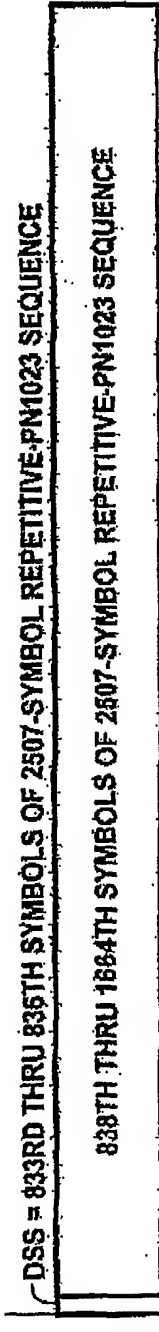


FIG. 3J

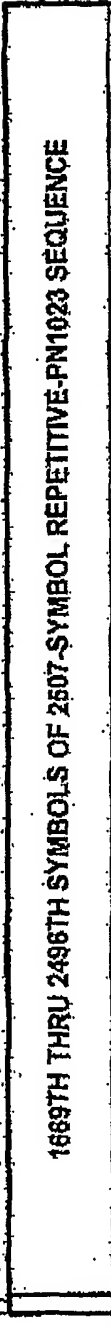


FIG. 3K

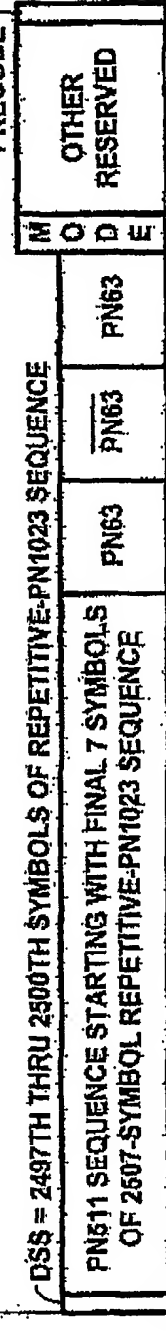
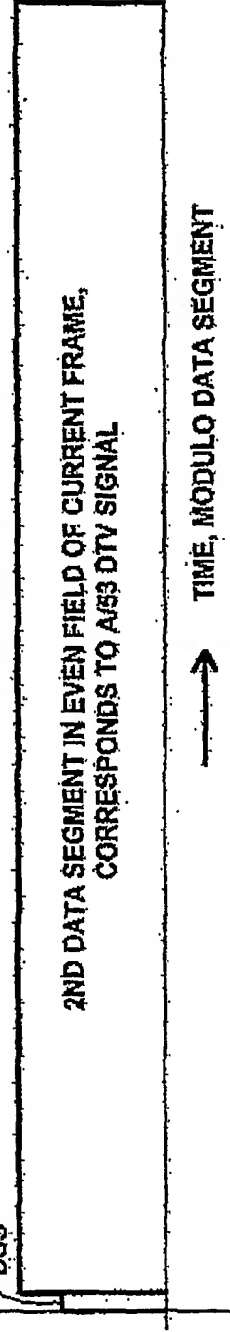
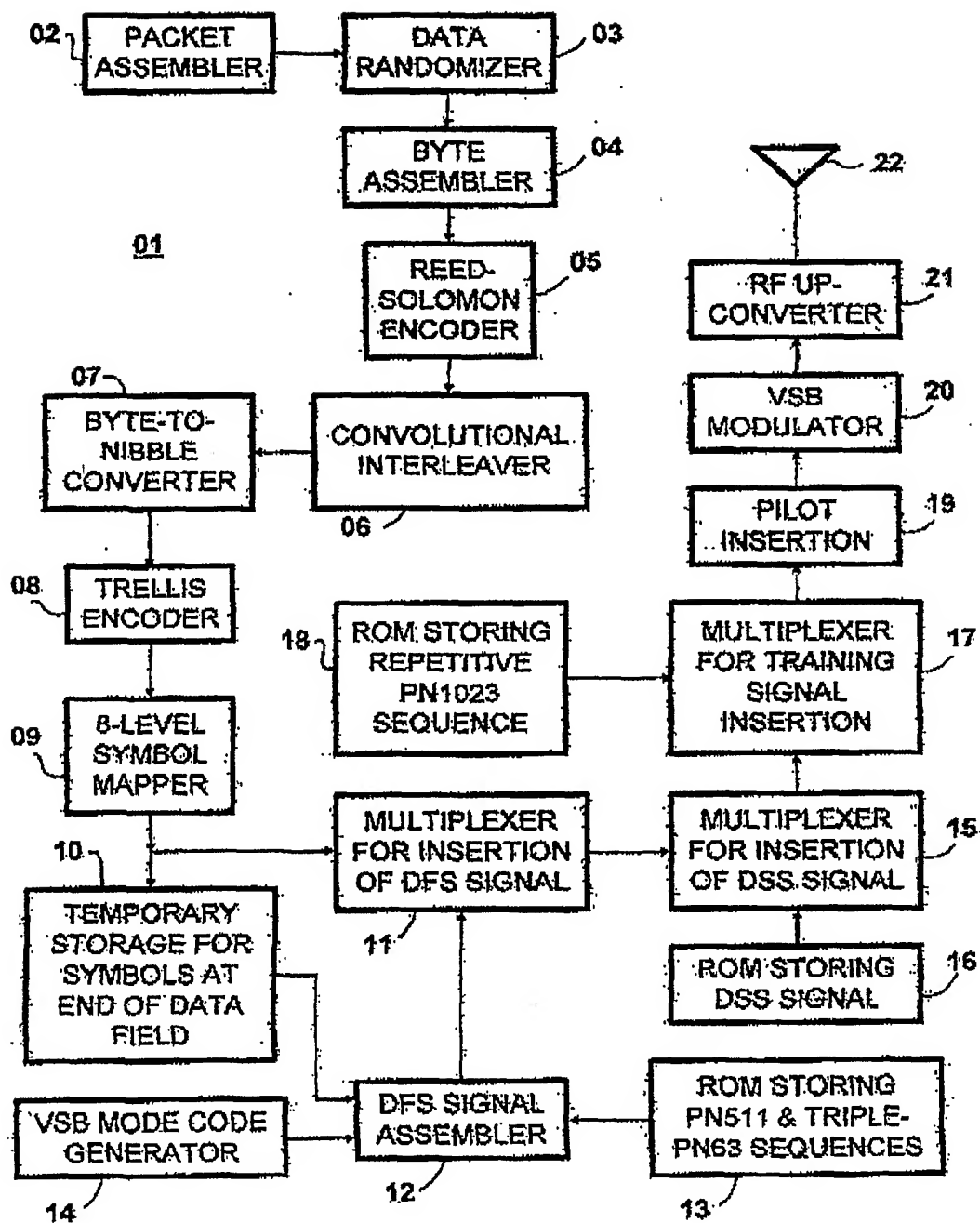


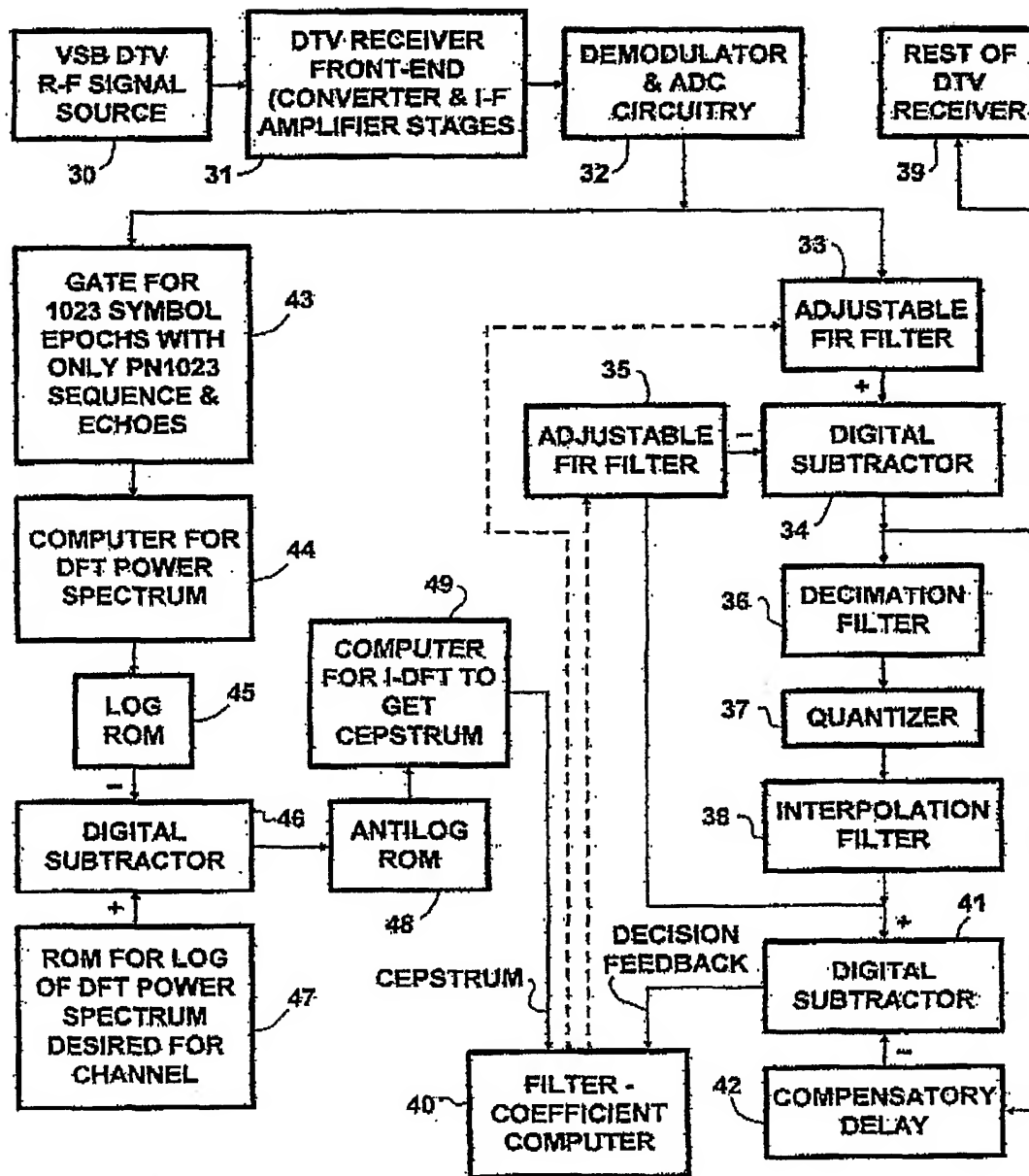
FIG. 3L



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FIG. 4

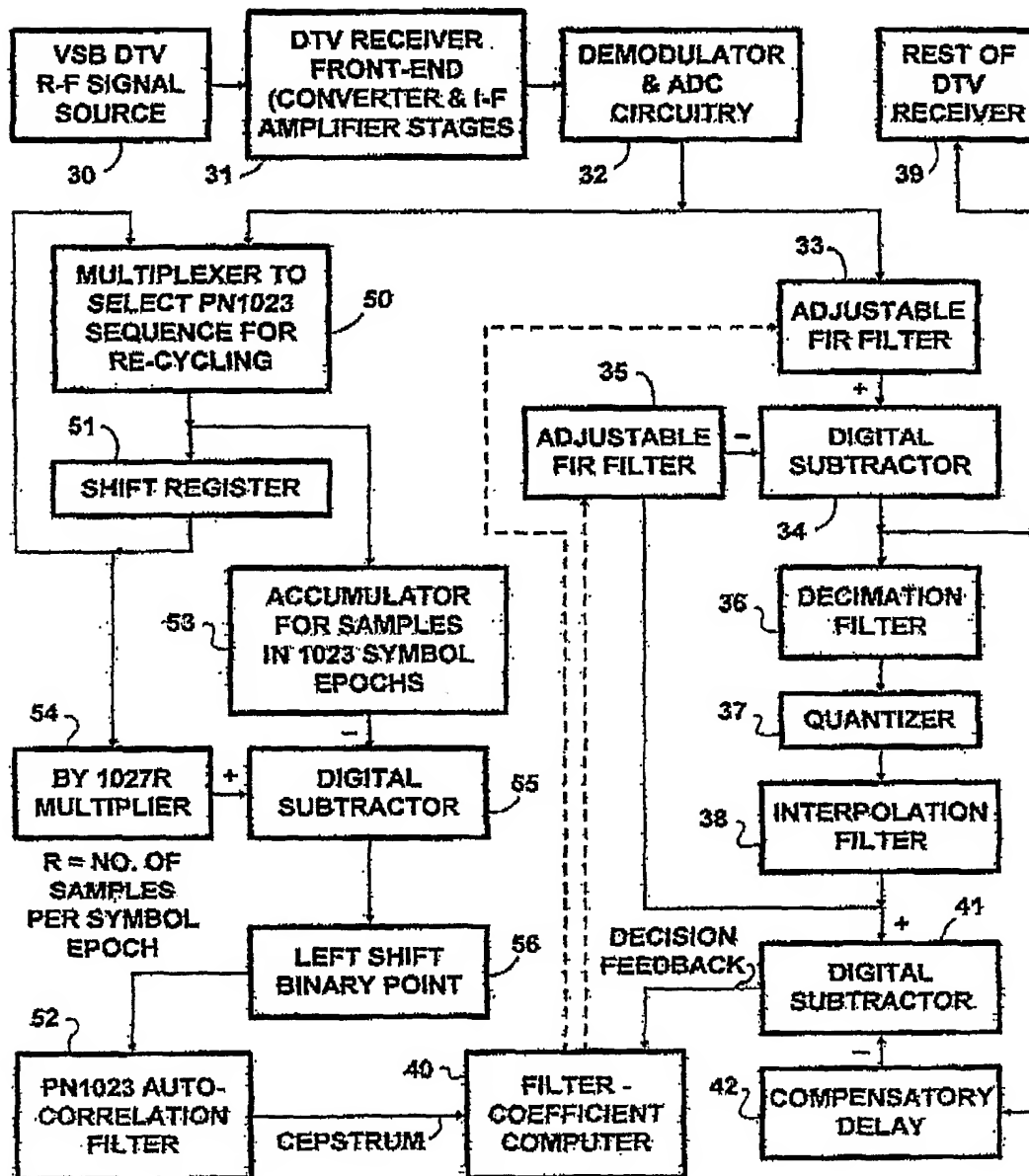
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FIG. 5



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FIG. 6



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FIG. 7

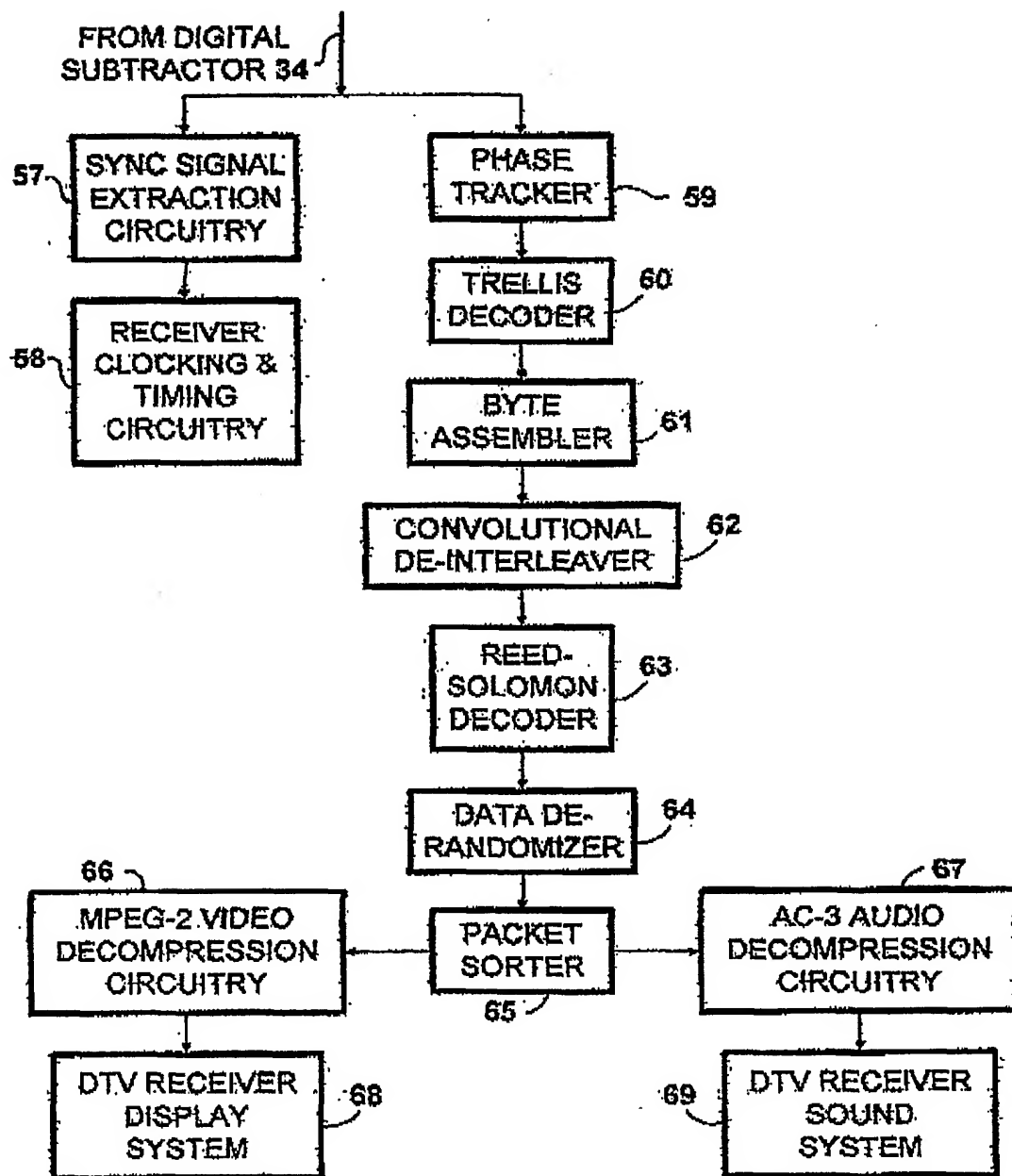


FIG. 8A

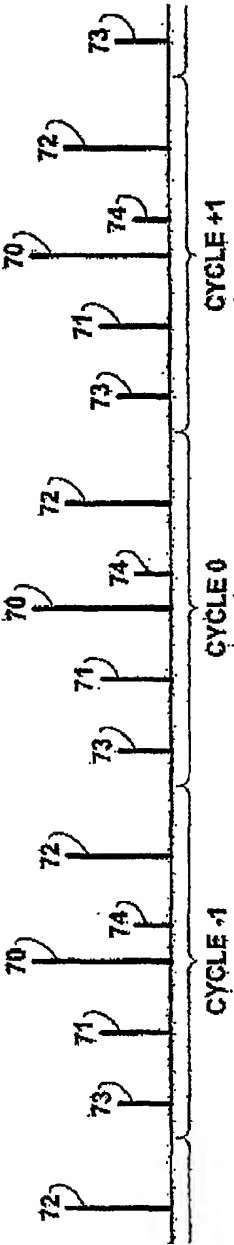


FIG. 8B

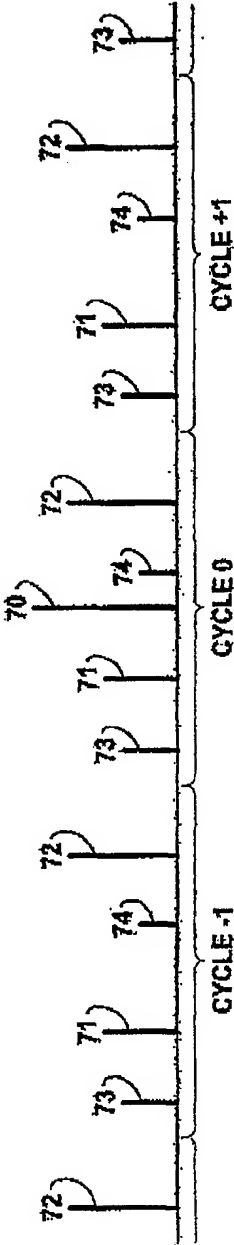


FIG. 8C

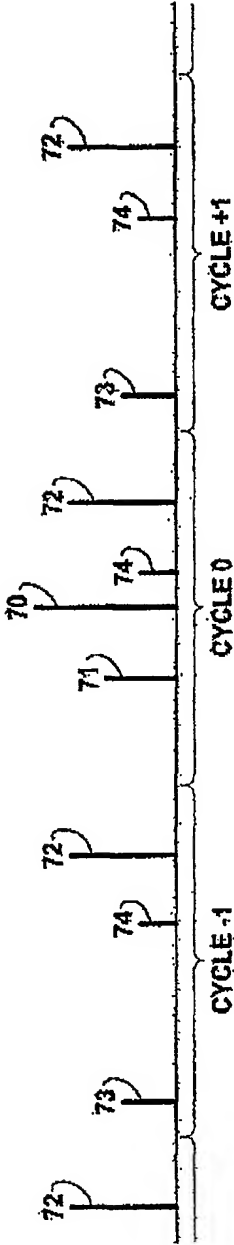
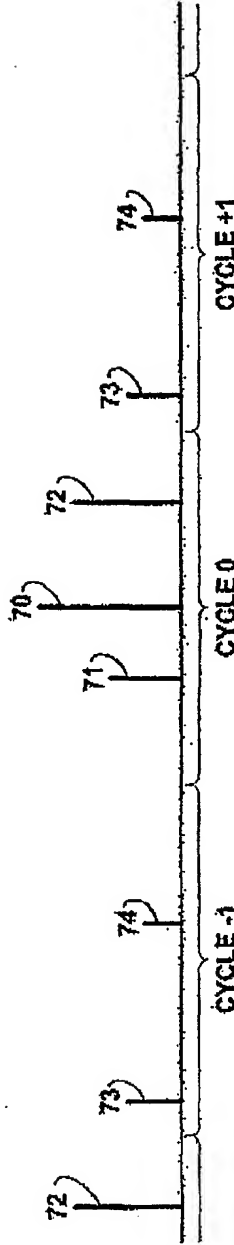


FIG. 8D



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FIG. 9

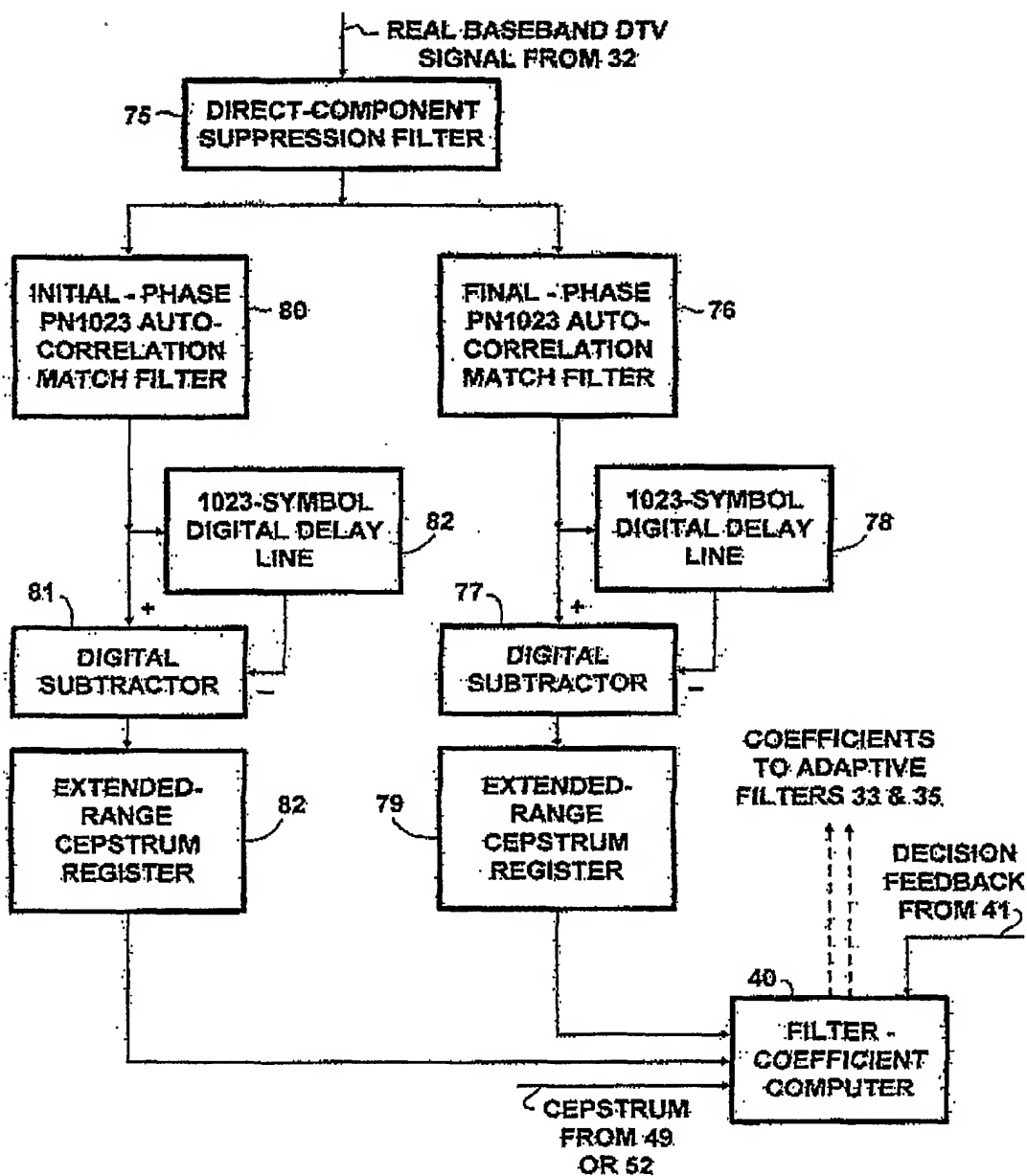


FIG. 10A



FIG. 10B

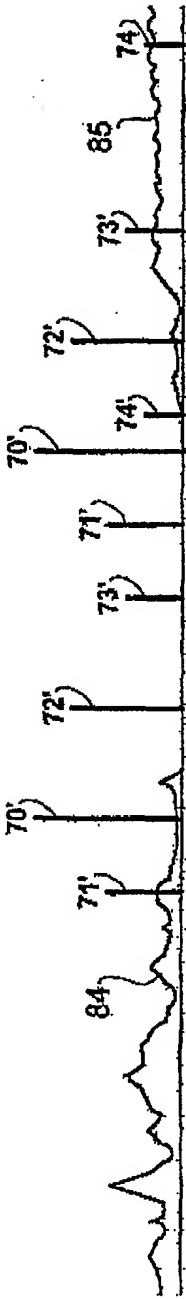
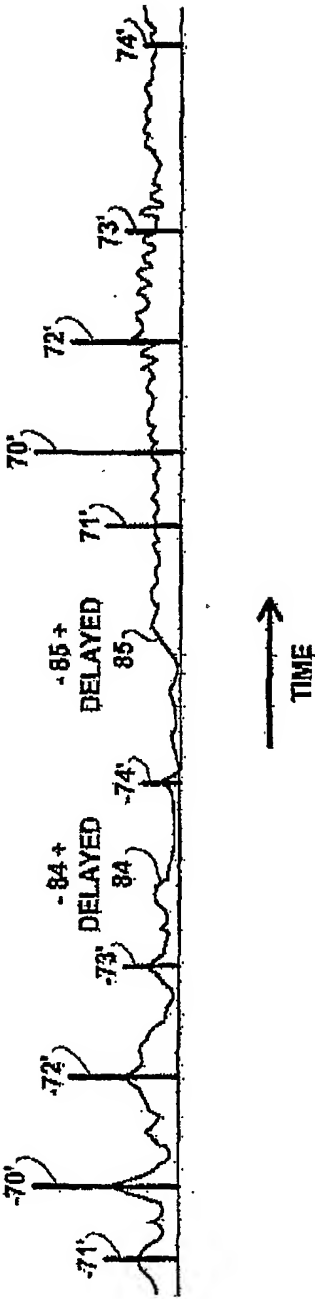


FIG. 10C



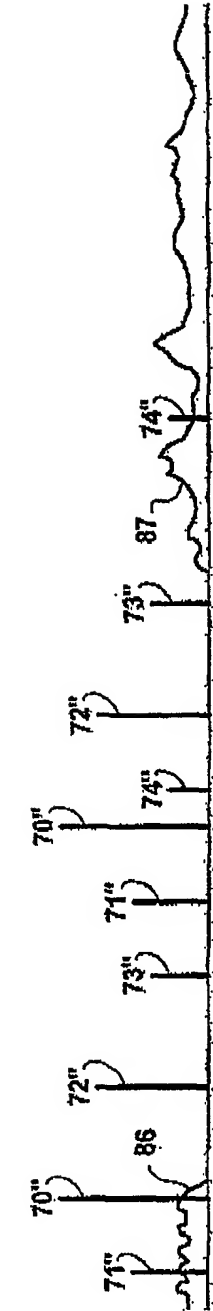


FIG. 10D

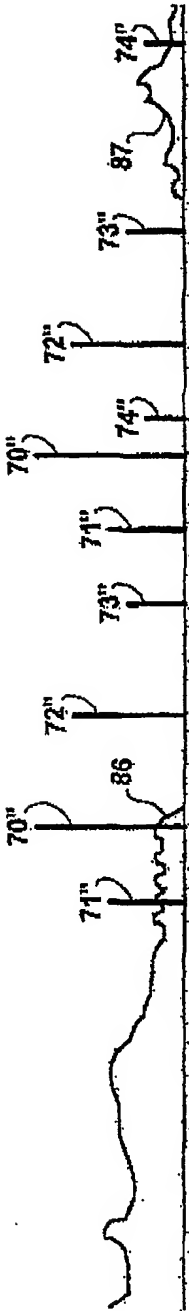


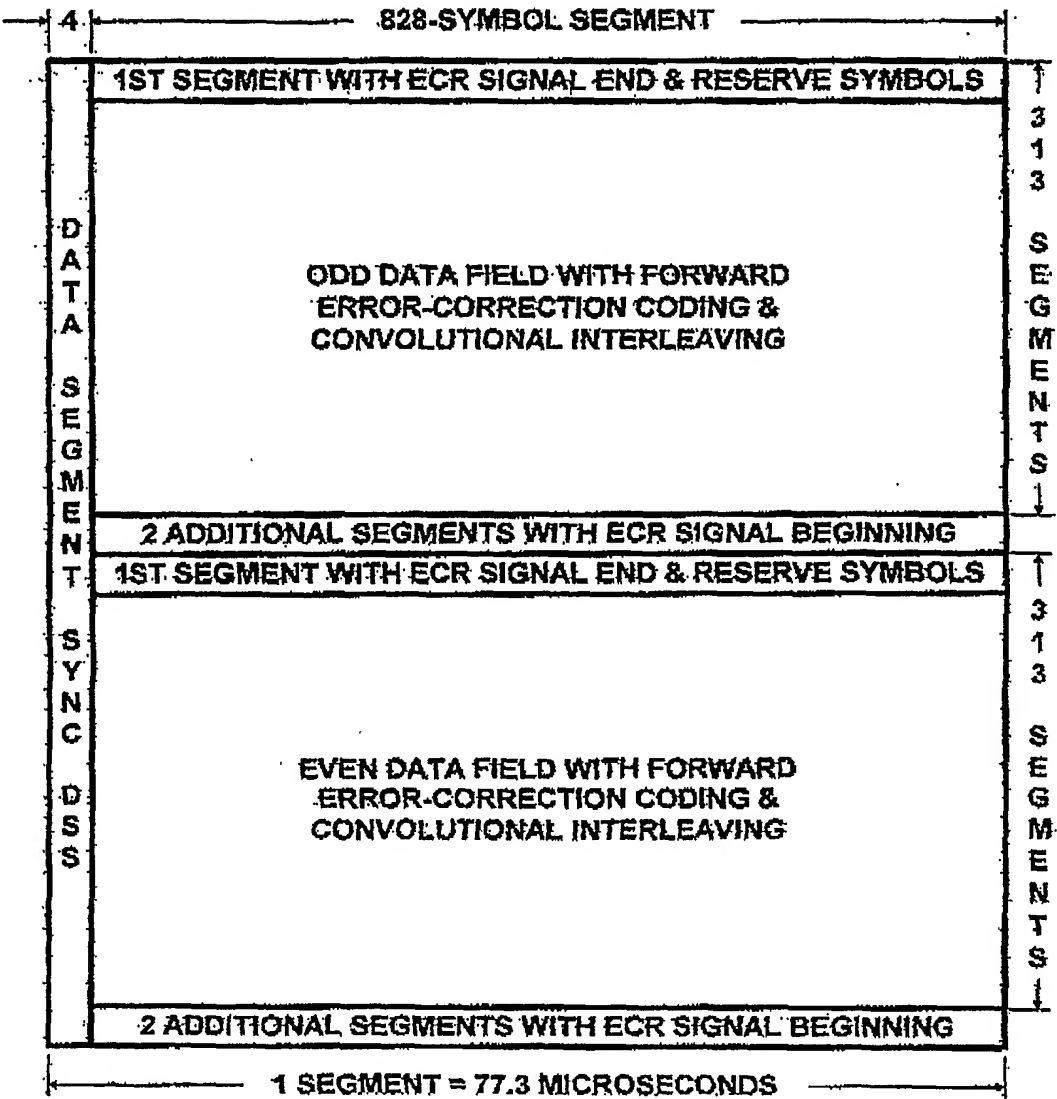
FIG. 10E



FIG. 10F

TIME

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FIG. 11



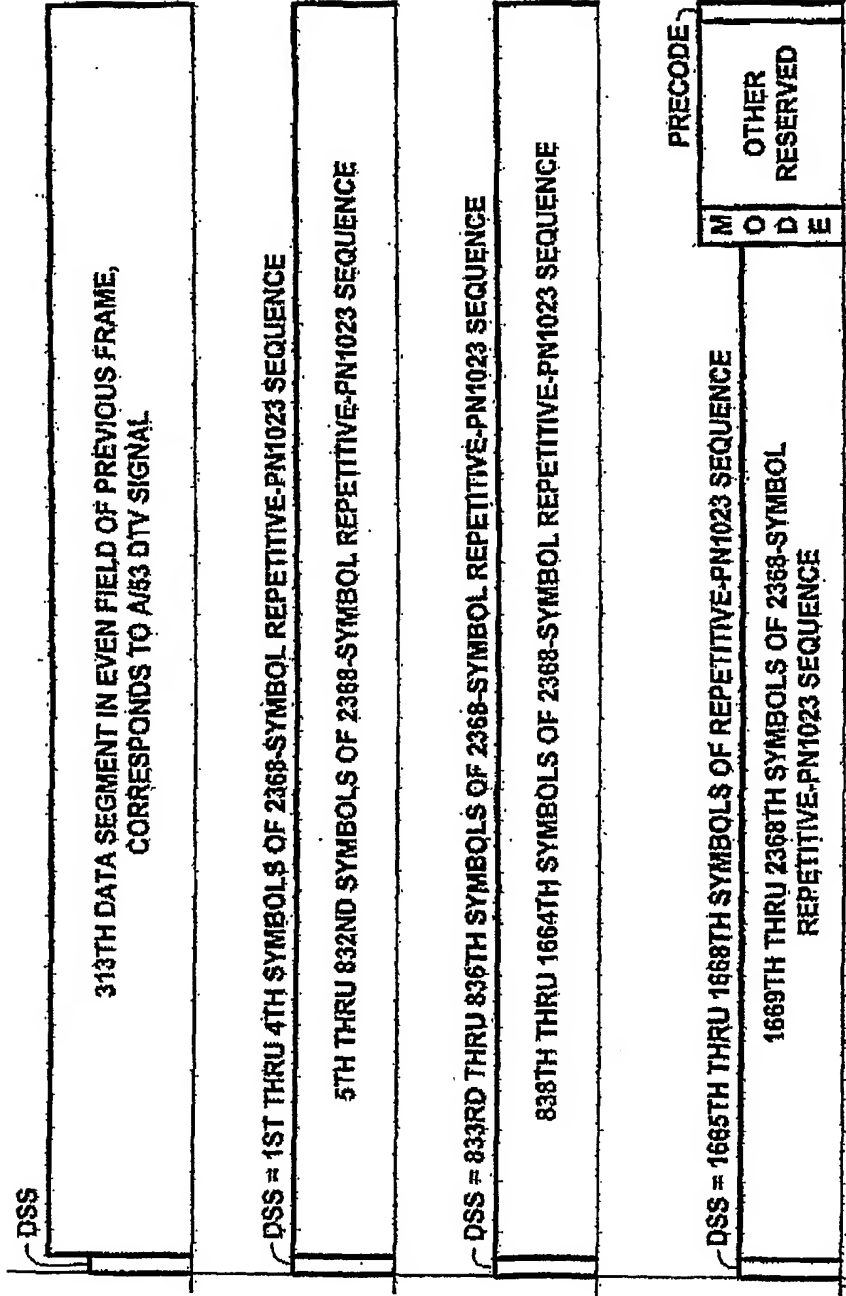


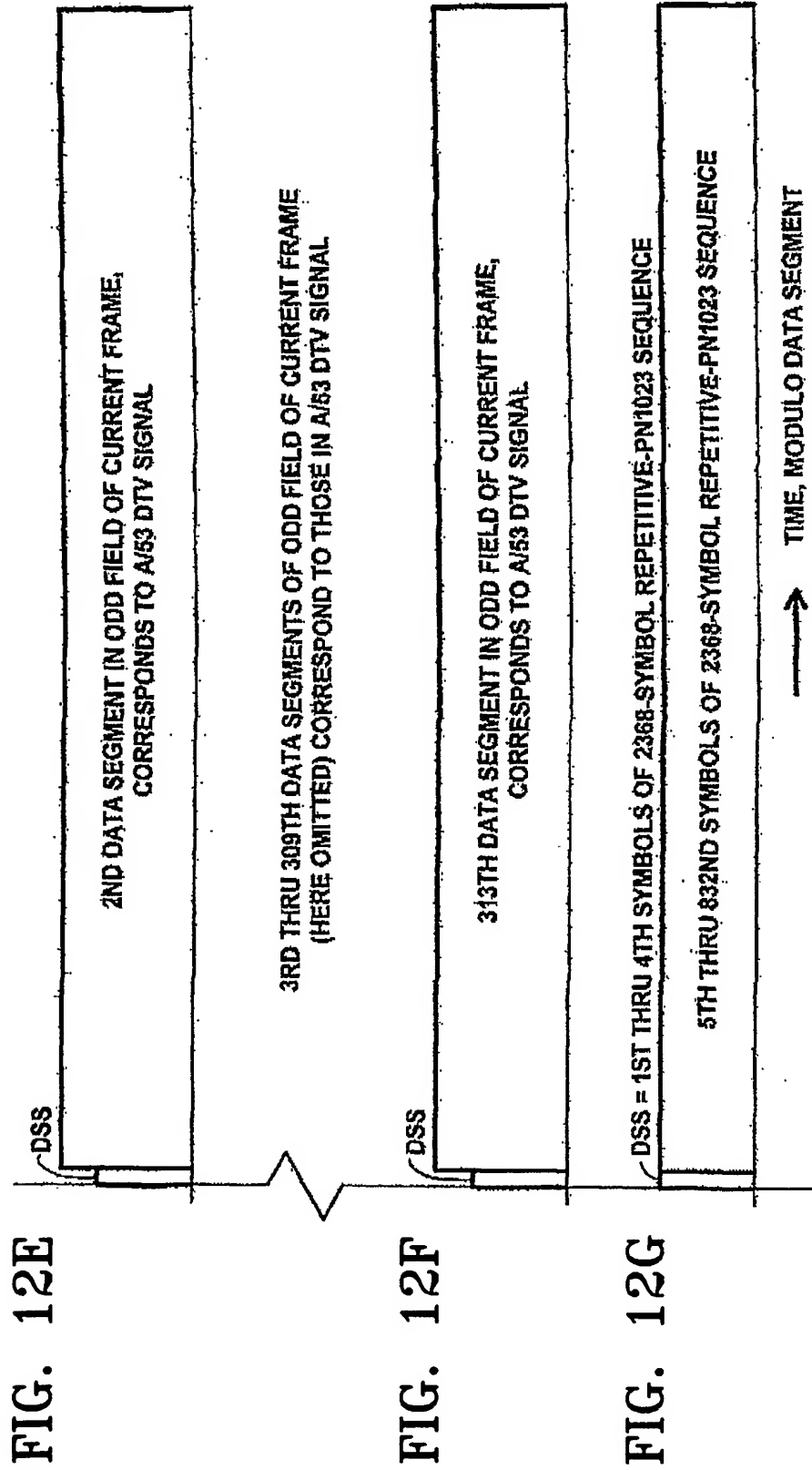
FIG. 12A

FIG. 12B

FIG. 12C

FIG. 12D

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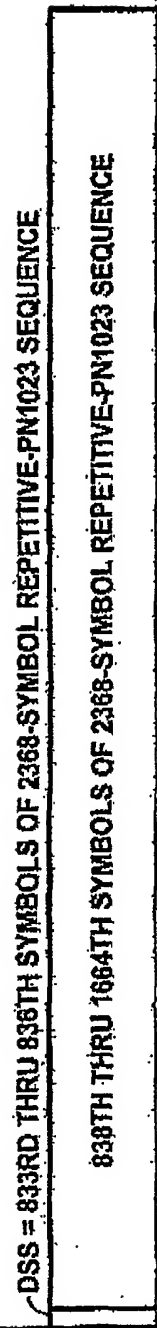


FIG. 12H

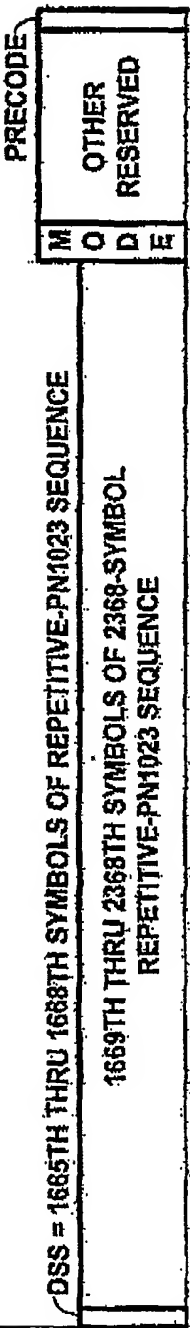


FIG. 12I

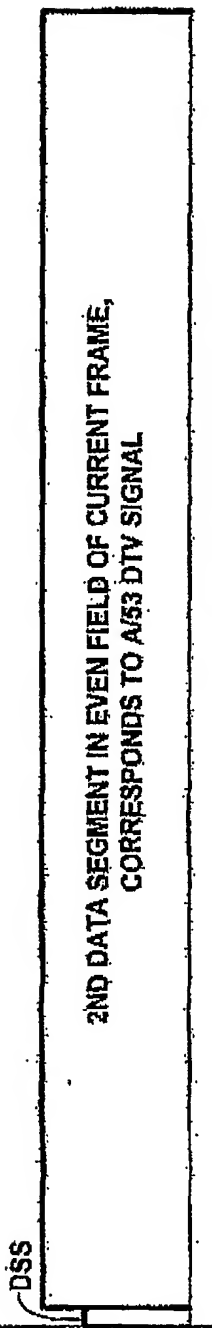


FIG. 12J

→ TIME, MODULO DATA SEGMENT

INTERNATIONAL SEARCH REPORT

International application No.
PCT/KR01/01190

A. CLASSIFICATION OF SUBJECT MATTER**IPC7 H04N 7/015**

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4,760,596 A (GTE Laboratories Incorporated, Waltham, Mass.) See the whole document	1
A	EP 0,884,886 A2 (Oki Electric Industry Co., Ltd.) See the whole document	1
A	KR 1999-0078413A (MOROLA INC,) See the whole document	1

☐ Further documents are listed in the continuation of Box C.☐ See patent family annex.

* Special categories of cited documents:

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 "O" document referring to an oral disclosure, use, exhibition or other means
 "P" document published prior to the international filing date but later than the priority date claimed

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 "&" document member of the same patent family

Date of the actual completion of the international search

23 OCTOBER 2001 (23.10.2001)

Date of mailing of the international search report

31 OCTOBER 2001 (31.10.2001)

Name and mailing address of the ISA/KR

Korean Intellectual Property Office
 Government Complex-Daejeon, Dunsan-dong, Seo-gu, Daejeon
 Metropolitan City 302-701, Republic of Korea

Facsimile No. 82-42-472-7140

Authorized officer

CHOI, Hoon

Telephone No. 82-42-481-5990



INTERNATIONAL SEARCH REPORT

Information on patent family members

international application No.

PCT/KR01/01190

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
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EP 0,884,886 A2	16. 12. 1988	JP 11004283A2	06. 01. 1999
KR 1999-0078413 A	25. 10. 1999	GB 9907069 A	19. 05. 1999
		GB 2336279 A1	13. 10. 1999